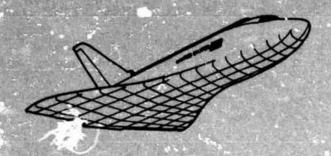


NASA CR-

141927



### DATA CORRELATION AND ANALYSIS OF ARC TUNNEL AND WIND TUNNEL TESTS OF RSI JOINTS AND GAPS

PHASE II FINAL REPORT

**VOLUME II -- DATA REPORT** PART 2 DRD MA-384T 19 MAY 1975

MCDONNELL DOUGLAS ASTRONAUTICS COMPANY . EAST

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CORPORATION

N75-28105 Unclas 31033 TESTS VCLUME 2: TUNNEL MIND

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#### **FOREWORD**

This report summarizes the work conducted by McDonnell Douglas Astronautics Company-East (MDAC-E) in St. Louis, Missouri for the Structures and Mechanics Division of the NASA Johnson Space Center (NASA-JSC) under Contract NAS9-14012, "Data Correlation and Analysis of Arc Tunnel and Wind Tunnel Test of RSI Joints and Gaps, Phase II." This final report consists of two volumes: Volume I - Technical Report and Volume II - Data Base, Part 1 and Part 2. The period of p rformance was from 20 May 1974 thru 19 May 1975.

Mr. Donald J. Tillian was the NASA Technical Monitor for this study; Messrs. H. E. Christensen and H. W. Kipp were the MDAC Principal Investigator and Study Manager, respectively. Significant contributions to this study were made by A. E. Bruns, M. B. Donovan, L. H. Ebbesmeyer, E. A. Eiswirth and T. W. Parkinson. The cooperation of numerous NASA Personnel at Ames Research Center, Johnson Space Center and Langley Research Center in providing experimental data, supplemental calculations and valuab! unsel was instrumental to the successful completion of this study. We are appreciative of the cooperation from the following for supplying test data; C. D. Scott and L. P. Murray of JSC, W. K. Lockman and F. J. Centolanzi of Ames, D. A. Throckmorton and I. Weinstein of LaRC, and G. W. Mauss and C. B. Blumer of Rockwell International.



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9.0-1 thru 9.0-2	*

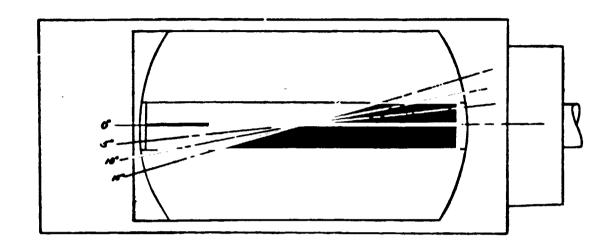


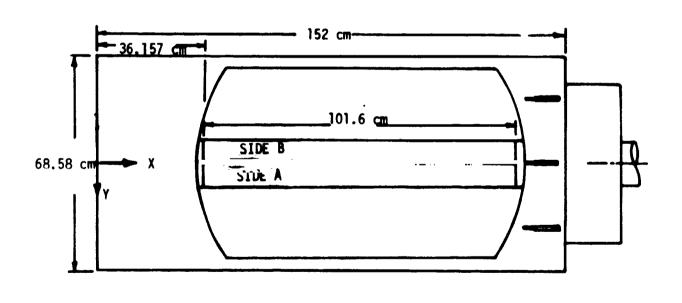
5.0 NASA/AMES, 3.5 FOOT H.W.T. TESTS OF LONG IN-LINE GAP

Thin skin models with a long in-line gap were tested in the Ames 3.5 foot H.W.T., Figure 5.0-1. Thermocouples were installed along the top of the panel and along the faces of the gap. These are shown in Section 5.1. Gap widths of zero, 0.127cm and 0.254 cm for a gap depth of zero, 1.0 cm, 2.0 cm and 3.81 cm and for a gap length of 101.6 and 30.48 centimeters were tested at 0, 5, 10 and 15 degree orientation to the flow. Tests were conducted at a free stream Mach number of 5.1 and Reynolds number per meter of  $1.64 \times 10^6$ ,  $3.28 \times 10^6$  and  $6.56 \times 10^6$ . Figure 5.0-2 is a complete run schedule.



### AMES 3.5 FOOT H.W.T. IN-LINE GAP MODEL









#### RUN SCHEDULE

SINGLE IN-LINE GAP TESTED IN THE AMES 3.5 H.W.T. MODEL OH-43

TEST SUPERVISED BY C. D. BLUMER

3 1.64 4 1.64 5 3.28 6 1.64 7 3.28 8 6.56 9 1.64 10 3.28 11 6.56 12 6.56 12 6.56 13 6.56 14 3.28 15 1.64 16 6.56 17 3.28 18 1.64 20 3.28 19 1.64 20 3.28 21 1.64 22 3.28 23 3.28 24 1.64 25 1.64 27 1.64 28 3.28 27 1.64 28 3.28 29 1.64 20 3.28 31 3.28 21 1.64 22 3.28 23 3.28 24 1.64 25 1.64 0.127 26 3.28 27 1.64 28 3.28 29 1.64 20 3.28 31 3.28 31 3.28 31 3.28 31 3.28 31 3.28 31 3.28 31 3.28 31 3.28 31 3.28 31 3.28 31 3.28 31 3.28 31 3.28 31 3.28 31 3.28 31 3.28 31 3.28 31 3.28 31 3.28 32 1.64 33 3.28 31 3.28 31 3.28 31 3.28 31 3.28 32 1.64 33 3.28 34 1.64 35 6.56 36 0.254 37 0.127 38 1.64 37 0.127 38 1.64 37 0.127 38 1.64 37 0.127 39 1 0.127		_	TEST	SUPERVI	ZED RA C	. D. BLU	IEK		
2 3.28 3 1.64 4 1.64 5 3.28 6 1.64 7 3.28 8 6.56 9 1.64 10 3.28 11 6.56 12 6.56 12 6.56 13 6.56 17 3.28 18 1.64 19 1.64 19 1.64 20 3.28 18 1.64 19 1.64 20 3.28 21 1.64 0.254 32 22 3.28 23 3.28 24 1.64 25 1.64 0.127 26 3.28 27 1.64 0.127 36 33 3.28 31 3.38 31 3.3			WIDTH	DEPTH	LENGTH	ORIENT.	T/C SCHEDULE	POSITION	REMARKS
35   6.56   1   0.254   37   38   39   1   1   5   5   5   1   3   3   3   3   3   3   3   3   3	NO.  1 2 3 4 5 6 7 8 9 10 11 2 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33	(X10 <sup>6</sup> /m)  1.64 3.28 1.64 3.28 1.64 3.28 6.56 6.56 6.56 3.28 1.64 3.28 1.64 3.28 1.64 3.28 1.64 3.28 1.64 3.28 1.64 3.28 1.64 3.28 1.64 3.28 1.64 3.28 1.64 3.28 1.64 3.28 1.64 3.28 1.64 3.28	0.127 0.254 0.127	DEPTH (cm)  0 2.032 0 3.81	101.6 30.48	ORIENT. ANGLE (DEG)  O	2 1 1 4 2 5D 3.3 6H	POSITION SCHEDULE	TUNNEL CONDITIONS UNSTEADY, WILL RE-RUN GAP FILLED WITH DENTAL PLASTER L.E.1 L.E.1
40 41 42 0.127	_35 36 37 38 39 40 41		0.127			5	61	3	



#### RUN SCHEDULE

SINGLE IN-LINE GAP TESTED IN THE AMES 3.5 H.W.T. MODEL OH-43

TEST SUPERVISED BY C. D. BLUMER

		1531	JOLEKAI	SED BL C	. D. DLU			
RUN NO.	R <sub>N</sub> (X10 <sup>6</sup> /m)	GAP WIDTH (cm)	GAP DEPTH (cm)	GAP LENGTH (cm)	GAP ORIENT. ANGLE (DEG)	T/C SCHEDULE	MODULE POSITION SCHEDULE	
43 44 45 46 47 48 49 50 51 52 53 54 55 57 58 59	1.64 3.28 6.56 1.64 3.28 6.56 1.64 3.28 1.64 3.28 1.64 3.28	0.254 0.254 0.063 0.254	2.037	101.6	10	3A 4 4 5D 15D		L.E.1 L.E.1
60 61 62 63 64 65 66 67 68 69	6.56 3.28 6.56 1.64 3.28 6.56 6.56	0.127	2.032 1.016 0.508		15 15 10 10 5 0	5D 3A		
71 72 73 74 75 76 77 78 79 80 81 82	3.28 1.64 3.28 6.56 1.64 3.28 6.56 1.64 3.28 3.28	0.127	9.381 0.381	30.48 (FWD)	5 + 10 + 15	5E 5F 5G	4	TOTAL TEMP.RAKE IN (MOD.6



#### RUN SCHEDULE

SINGLE IN-LINE GAP TESTED IN THE AMES 3.5 H.W.T. MODEL OH-43

TEST SUPERVISED BY C. D. BLUMER

RUN NO.	R <sub>N</sub> (X10 <sup>6</sup> /m)	GAP WIDTH (cm)	GAP DEPTH (cm)	GAP LENGTH (cm)	GAP ORIENT. ANGLE (DEG)	T/C Schedule	MODULE POSITION SCHEDULE	REMARKS
83 84 85 86 87 88 89 90 91 92 93	3.28 3.28 1.64 1.64 3.28 6.36 1.64 3.28 6.56 6.56 6.56	0.127 0.254 0.127 0.254	2.032	30.48 (FWD) 30.48 (AFT)	15 0 15	5G 5E 5H	4	



5.1 Model Description and Instrumentation Location - The test configuration consisted of a thin skin model inserted into a 68.6 x 152.4 cm carrier plate wedge. Figure 5.0-1 shows the model inserted in the carrier plate. The joint configuration was a single, in-line, gap of either 30.48 cm (12 in) or 101.6 cm (40 in) length. The test matrix included four flow orientations, three gap widths, and four gap depths. A run schedule is given in Figure 5.0-2 which defines the test conditions (i.e., gap width, depth, length, etc) for each run.

The model was heavily instrumented to obtain heating data in the presence of laminar, transitional and turbulent boundary layers, and to investigate the effect of tile orientation for several gap width settings. Instrumentation included total temperature and pressure probes to define the free stream conditions, thermocouples along the gap length to define surface and gap heating, and instrumented modules to further define heating distributions.

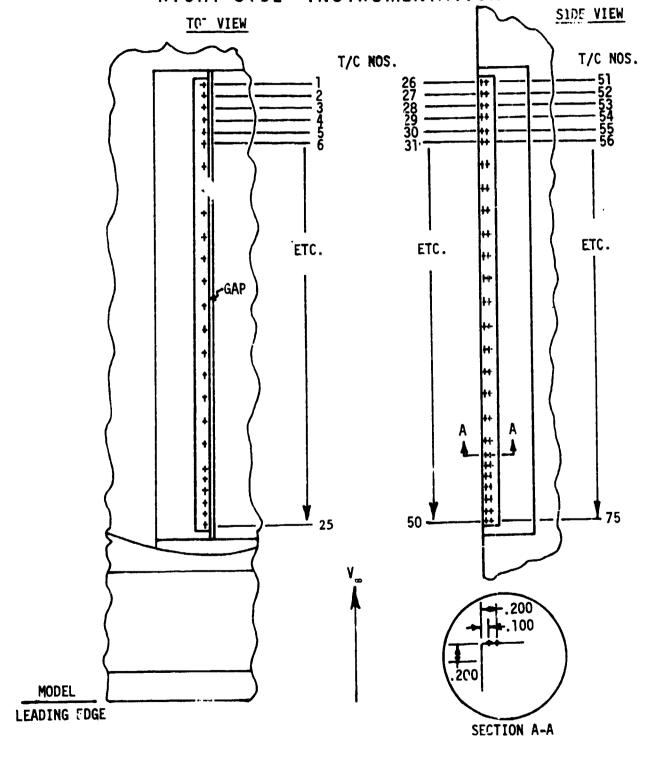
The total temperature and pressure probes were mounted on the downstream end of the wedge at three spanwise (Y) locations as seen in Figure 5.0-1. These probes were used to define the free stream conditions for each test run.

The thermocouples along the gap length are shown graphically in Figure 5.1-1. This instrumentation consisted of one row of thermocouples along the top surface of tile at Y = -0.200 in and two rows of thermocouples near the top of the gap at depths (2) of 0.100 and 0.200 inch. Each row contained 25 thermocouples. The axial location of each thermocouple is given in Figure 5.1-2.

Thermocouple locations on the instrumented modules are given in Figure 5.1-3 for each of the modules used. During the test program, five different module arrangements or positions were employed as defined in Figure 5.1-4. This figure gives for each arrangement, the instrumented modules used and their axial location. The reader is referred back to the run schedule (Figure 5.0-2) which cross-references the module position used during each run. It is noted, that not all available thermocouples were connected during a run. The thermocouple hookup schedule is given in Figure 5.1-5, and again the reader is referred to Figure 5.0-2 to determine the applicable T/C schedule for each run.

Nominal gap widths investigated during the test program were 0, 0.025, 0.050 and 0.100 inches. For each run, the actual gap width was measured at various axial locations, and are recorded in Figure 5.1-6.

### AMES 3.5 FOOT H.W.T. IN-LINE GAP MO € L RIGHT SIDE INSTRUMENTATION



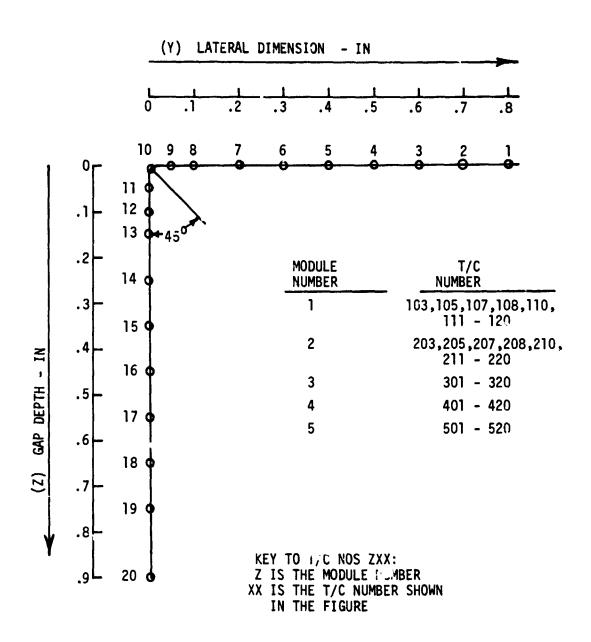


### THERMOCOUPLE LOCATIONS AMES 3.5 FOOT H.W.T. INLINE GAP MODEL

	AMES	3.5	FOOT H.W	T. INLINE		DEL
T/C	NUMBERS		X <sub>1</sub> DISTANCE	FROM	X <sub>2</sub> Dist <b>a</b> nc	F FROM
ROW 1	ROW 2	ROW 3		EDGE (IN)		
ROW 1  1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25	ROW 2  26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50	FOW 3 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75	LEADING  53.24 52.24 51.24 50.24 49.24 48.25 46.24 44.24 42.24 40.23 38.23 36.23 30.23 28.23 20.23 21.23 21.23 21.23 21.23 22.23 27.23 28.23 28.23 29.23 29.23 29.23 29.23 29.23 29.23 29.23 29.23 29.23 29.23 29.23 29.23 29.23 29.23	4 66 66 77 99 99 22 77 77 77 77 77 77 77 77 77 77	39. 38. 37. 36. 35. 30. 28. 26. 24. 22. 10. 8. 5. 5.	011 011 012 014 015 014 007 012 002 002 003 003 002 002 002
		14.	235IN			
٧ <sub>∞</sub>	Y	X			JT/C1	IN-LINE GAP



# THERMOCOUPLE LOCATIONS ON THE INSTRUMENTED MODULES AMES 3.5 FOOT H.W.T. IN-LINE GAP MODEL



33

က

ARRANGEMENT #3

MOD.

4.5

MOD. ARRANGEMENT #2

MOD. ARRANGEMENT #1

Ź,

FIGURE 5.1-4 CONC.

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### THERMOCOUPLE HOOKUP SCHEDULES AMES 3.5 FOOT H.W.T. IN-LINE GAP MODEL

T/C HOOKUP SCHEDULE NO.	T/C NUMBER	NUMBER OF T/C'S
1	1 - 75	75
2	1 - 25 103,105,107,108,110, 203,205,207,208,210 301 - 310 401 - 410 501 - 510	65
3 <b>A</b>	1 - 25 103,105,107,108,110,111 - 115 203,205,207,208,210,211 - 215 306 - 315 406 - 415 506 - 515	75
4	102,105,107,108,110, 111 - 120 203,205,207,208,210, 211 - 220 306 - 320 406 - 420 506 - 520	75
5D	1 - 25 103,105,107,108,110, 111 - 115 203, 205, 207, 208, 210, 211 - 215 306 - 320 506 - 520	75
5E	6 - 25 103,105,107,108,110, 111 - 115 203,205,207,208,210, 211 - 220 306 - 320 506 - 515 601 - 605	75
5F	16 - 25 41 - 50 103,105,107,108,110, 111 - 115 203,205,207,208,210, 211 - 220 306 - 320 406 - 415 601 - 605	75



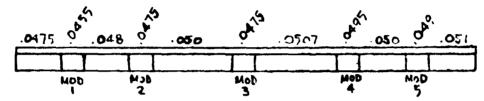
### THERMOCOUPLE HOOKUP SCHEDULES AMES 3.5 FOOT H.W.T. IN-LINE GAP MODEL

T/C HOOKUP SCHEDULE NO.	T/C NUMBER	NUMBER OF T/C'S
5G	16 - 25 41 - 50 103,105,107,108,110, 111 - 115 203,205,207,208,210, 211 - 220 306 - 320 506 - 515 601 - 605	75
5Н	1 - 15 103,105,107,108,110, 111 - 115 306 - 320 406 - 420 506 - 520 601 - 605	75
6Н	6 - 25 103,105,107,108,110, 111 - 120 203,205,207,208,210, 211 - 220 406 - 420 506 - 515	. 75
61	16 - 25 41 - 50 103,105,107,108,110, 111 - 115 203,205,207,208,210, 211 - 220 405 - 420 506 - 520	75
6J	1 - 15 103,105,107,108,110, 111 - 120 203,205,207,208,210, 211 - 220 406 - 420 506 - 520	75
15D 5D WITH SINGLE GAP PROBE INSTEAD OF T/C 213	1 - 25 103,105,107,108,110, 111 - 115 203,205,207,208,210,211,212, GAF 214,215 306 - 320 506 - 520	75 P TOTAL TEMP. PROBE (CALLED GAP)

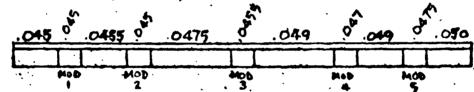
REPORT MDC E1248 JSC 09651

# MEASURED GAP WIDTHS AMES 3.5 FOOT H.W.T. IN-LINE GAP MODEL

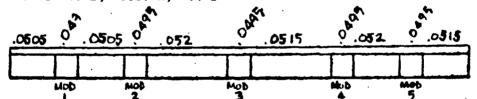
- o SKETCHES NOT TO SCALE
- o ALL DIMENSIONS IN INCHES
- 1) RUNS 6-11 40"L, .050"W. .8"D



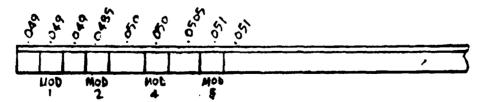
2) kuns 13-15 40"L, .050"W, 1.5"D



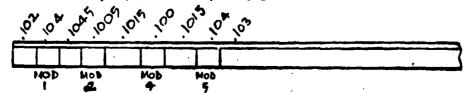
3) KUNS 16-18 40"L, .050"W, .4"D



4) Rens 19-20 12"(FWD)L, .050"W, .8"D



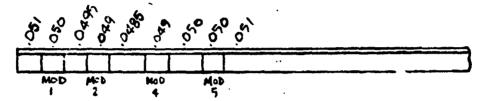
5) RUNS 21-24 12"(FWD)L, .100"W, .8"D



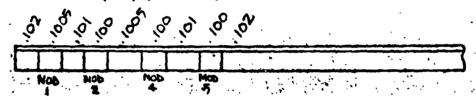


## MEASURED GAP WIDTHS AMES 3.5 FOOT H.W.T. IN-LINE GAP MODEL

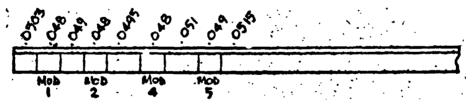
- o SKETCHES NOT TO SCALE
- o ALL DIMENSIONS IN INCHES
- 6) RUNS 25-28 12"FWD)L, .050"W, .8"D



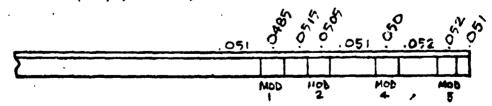
7) RUNS 29-32 12"(FWD)L, .100"W, .8"D



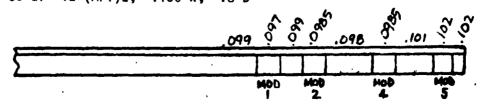
8) RUNS 33-34 12"(FWD)L, .050"W, .8"D



9) RUN 35 12"(AFT)L, .050"W, .8"D



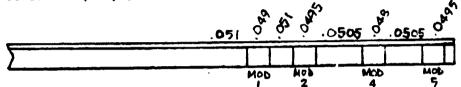
10) RUNS 36-37 12"(AFT)L, .100"W, .8"D



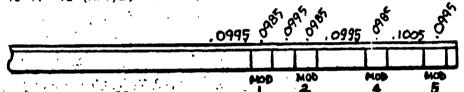


### MEASURED GAP WIDTHS AMES 3.5 FOOT H.W.T. IN-LINE GAP MODELS

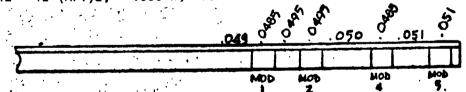
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- o ALL DIMENSIONS IN INCHES
- 11) RUNS 38-39 12"(AFT)L, .050"W, .8"D



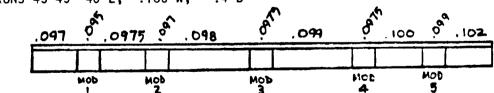
12) RUNS 40-41 12"(AFT)L, .100"W, .8"D



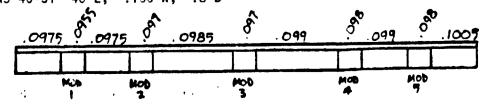
13) RUN 42 12"(AFT)L, .050"W, .8"D



14) RUNS 43-45 40"L, .100"W, .4"D



15) RUNS 46-51 40"L, .100"W, .8"D

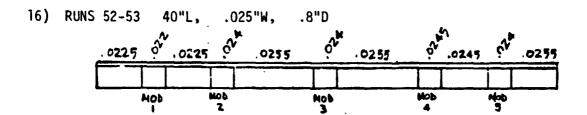


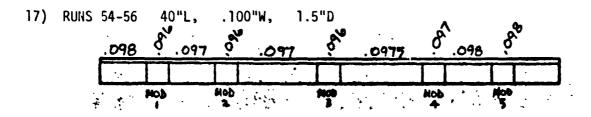
5.1-11

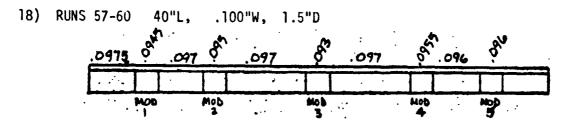


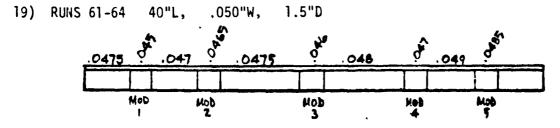
# MEASURED GAP WIDTHS AMES 3.5 FOOT H.W.T. IN-LINE GAP MODEL

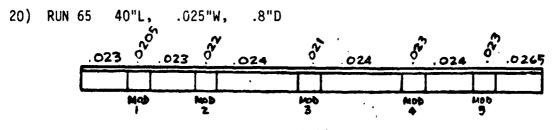
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- o ALL DIMENSIONS IN INCHES











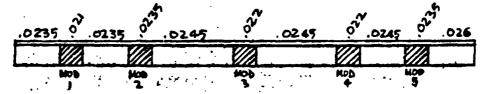
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# MEASURED GAP WIDTHS AMES 3.5 FOOT H.W.T. IN-LINE GAP MODEL

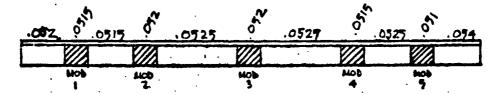
- o SKETCHES NOT TO SCALE
- o ALL DIMENSIONS IN INCHES
- 21) RUNS 66-68 40"L, .025"W, .4"D

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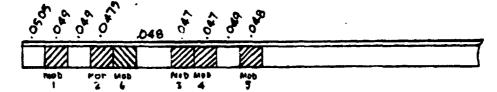
22) RUNS 69-71 40"L, .025"W, .2"D



23) RUNS 72-74 40"L, .050"W, .2"D



24) RUNS 75-83 12"(FWD), .050"W, 1.5"D



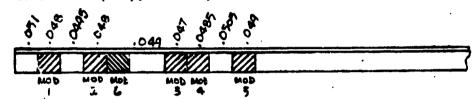
25) RUNS 84-88 12"(FWD), .100"W, 1.5"D



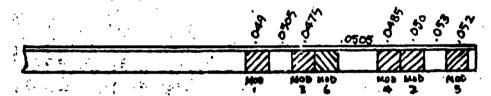
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# MEASURED GAP WIDTHS AMES 3.5 FOOT H.W.T. IN-LINE GAP MODEL

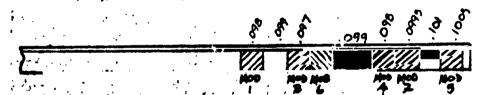
- o SKETCHES NOT TO SCALE
- o ALL DIMENSIONS IN INCHES
- 26) RUNS 89-90 12"(FWD), .050"W, .8"D



27) RUNS 91-92 12"(AFT), .050"W, 1.5"D



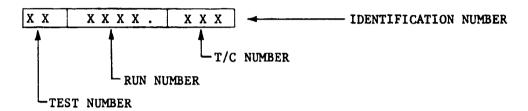
28) RUN 93 12"(AFT), .100"W, 1.5"D





5.2 Explanation of Terminology Used in Data Listing - Results from the Ames long in-line gap tests presented in Section 5.3 are organized by run number and contain information about test conditions, model configuration and thermocouple location, heat transfer parameters and boundary layer parameters. The data listing was prepared by analyzing and combining information recorded during calibration and test runs with boundary layer information.

The terminology used in the data listing is as follows:



A(RAD)

= Flow orientation - radians

B.L.

Boundary layer state (1=laminar, 2=transitional, 3=turbulent)

**DELS** 

Displacement thickness

FLOW-L

= Gap flow length

GAP

Gap width

GAP-D

Gap depth

G-CF

Gap configuration

HAW/HT

= Recovery factor (adiabatic wall enthalpy ratioed to free

stream total enthalpy)

0.908 for HT (Turbulent convective heat transfer coefficient)

0.874 for HL (Laminar convective heat transfer coefficient)

HL

= Convective heat transfer coefficient based on recovery

factor of 0.874

HLC, HLCC

= Conduction corrected HL

HL/HLCC

Convective heat transfer coefficient ratioed to conduction

corrected heat transfer coefficient

HL/HE

Convective heat transfer coefficient ratioed to heat transfer

coefficient measured on top of tile near gap

HLC/HEC

Conduction corrected HL/HE

HREF

- Convective heat transfer coefficient on calibration plate

HLC/HREF, HLCC/HREF = Conduction corrected HL ratioed to

heat transfer coefficient on calibration plate

# RSI GAP HEATING ANALYSIS - II

HL/HREF

Convective heat transfer coefficient in gap ratioed to coefficient on calibration plate at the same location

HT

- Convective heat transfer coefficient based on recovery factor of 0.907

LOC

Instrumentation location

M, MACH

Mach number

M-THICK

Momentum thickness

NSTT

Stanton number based on free stream conditions and HT

NTOL

Data sequence number

PATN

= Tile pattern (0=staggered, l=in-line)

PT

Free stream total pressure

Q

= Convective heating

OS

Heating rate to a sphere

RE/M, RE/METER

Unit Reynolds number per meter

RHO VEL

= Free stream density - velocity product

STEP

= Step height

STL

Stanton number based on free stream conditions and HL

STT

Stanton number based on free stream conditions and HT

SUB-T

= Sub-layer thickness

T

= Temperature of model at time test data was obtained

TT

= Free stream total temperature

T/C

= Thermocouple number

TW/TE

Temperature ratio across boundary layer

X

= Distance downstream from leading edge of carrier plate

X(BAR)

= Distance from leading edge of tile

Y, YY

= Lateral distance from tile centerline

z,zz

Distance from top of tile (X, Y, YY, Z, ZZ form right hand

coordinate system)



5.3 Data Tabulation for Ames 3.5 Foot H.W.T. Long In-Line Gap Heating Tests - This section contains the program for transcribing data from the Ames 3.5 Foot H.W.T. into the Data Bank and the tabulation generated by the program. The program listing is included for completeness and also documents those steps necessary to process the data into the Data Bank. The data listing begins on Page 5.3-22. This listing employs the "24 Attribute Word List" (described in Volume 1, Section 5) used in the data selection and data correlation programs.

# RSI GAP HEATING ANALYSIS - II

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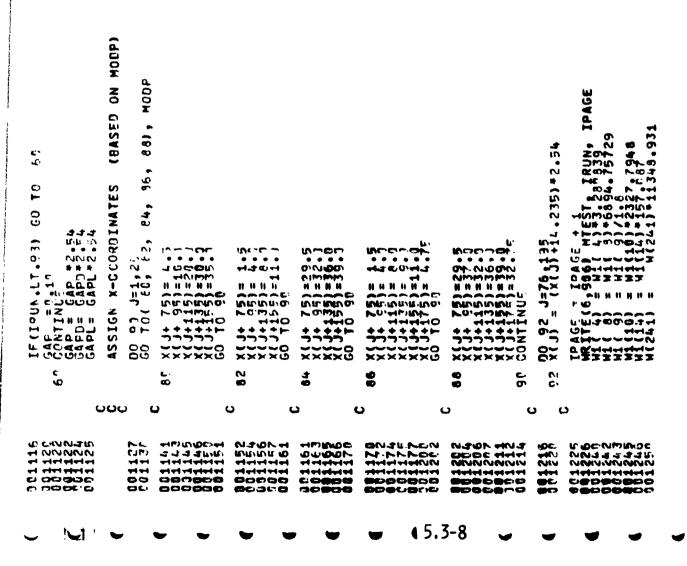
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JJ, JJ, JJ, J, I, CP, TAM, K(J), K( J+E41), H1 (14), H0ZRCP QRT(DIST2(1))\*SIGN1 GRT(DIST2(2))\*SIGN2 2(1)-01ST2(2) (T(1)/(X1MX2\*DIST2(1)) - T(2)/(X1MX2\*DIST2(2)) (T(1)/(DIST2(1)\*DIST2(2))) 2,1,0101,0210Y2,AB,CCN1 387 CF AIR OFUER CURVE 10 9 S CONDICTION EG.0.03 1.99672 = [.6254\*7861.1159/10?
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SLUMER, IN-LINE PSI GAP	±	(KG/H2-S)	6.37E-03	5.346-03	£ -36E-33	6.51E-03	7.506-53	3-126-03		20-2264	10476-02	1.406-62	1.568-02	1.436-02	1.366-02	1.216-02	1.116-12	A.32E-03	f. 6 15-83		2.40E-02	2.576-12	2.56E-02	2.438-62	2.416-92	2.32E-52	2.128-12	1.716-82	1.216-92	1.116-72	
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### REI GAP HEATING ANALYSIS - II VOLUME II

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H BOS CEST SMILE		COOD HARMANA IN TARBULE	/HREFFE 6.3	5.24 AUDITER 6.242	01300 +L12747 TH 75+3779	/HREFFT #.15C	BREFET 1 /NREFFE 7.9.8	BOFFE W. MARFFE 7.435	FLACEFU W. JHOSEFFE 7.F.1"	SPACE NI CHAFFEE	1000 1000 1000 1000 1000 1000 1000 100	CTURCE C HULLIAN CE TEST	CHURCH WINDERS ALTON	CHUSCHE BUSINESS II PERMERT	PARTY HARACKY IN THE PROPERTY OF	PRESENT MY /HARFFF F. F. L. L.	1-3-25° × Edukh/ In 14-361-	Caring HI FHATEE E.Ting . 9	and seet 2 HL /Hackfr 6.438t-	124E+E H. /HOEFFE B.C1TE-	Treatry W /Harffe 0.211E-1	"22EE+12 HL PHREFFE 0.1"	2515+12 HL /H25FF= 6493	STATES HE ANDTHE COUSE	3.2E+C2 HL /HREFFE 0.4	STOTE OF ME INSTERE	•	Z HANGER TH TI-EBAC.	[]+[]*[	LITE - Addition/ In 17+25-9"	SAME THE PROPERTY 74050	- (*) In (m)	3 H	L PARTITION
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	/HCC		. 968		70.	.987	. 988	.987	.417	196	.942	.980	.972	.967	946.	.930	6+5.	1.010	1.010	1.010	1.013	1.088	1.020	1.008	1.009	1.006	666.	.976	•	.974	086	196.	.979	646	.974	.973	.972	.967	.987	.929	.691	968.	1.021	1.023
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	HREF	(KG/M2-S)	•	•	* 20 / E=2	. 695E-02	.589E-02	.263E-C2	. £ 91E-12	1856-67	7:-3662	4075-12	. 26 CE-C2	. C B V E + C 3	. 528E-11	.353E-1 3	.293E-13	1-3763	.917E-03	37E-02	.101E-C2	. 17 2E - 9 2	10-35 );	.247E-52	*245E-02	. 323E-(2	~	~	4.7	6,1			•••	٠,	1.1	792E-63	.92E-32	23-2452	0 0 2 E - 0 3	C-3006	332E-7	2786-17	526E-11	0-3513
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	-	3	œ.	323.6	329.6	323.1	313.6	319.5	323.0	9.61	119.7	319.6	120.3	320.1	313.7	1.017	120.5	319.5	319.5			313.1	317.6	317.6	1130	31.9.1	314.2	1.7.7	317.2	, , , , , , , , , , , , , , , , , , ,	11.		317.8	317.5	316.7	310.5	315,4
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	(KG/M2-5)							1.tg4E-12		£ 395-62	8.372E-P2	€.:63F-02	7.926F-02	7.5886-02	7.35 E-02	6.752E-02	5.877F-C2	.8246-02	. 353E-02	.14 JE-n2	.527E-02	2.7866-12	. 716E-02	1.4926-02	354E-22	.327E-02	.3836-92	. e. 63E-62	5626-02	*C00E-02	1.6326-02	60-3734	3 3 3 3
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PAGE	HL/HLCC H	1.830					1.085	1.000	1.000	1.1	1.000	1.000	1.10									1.493	1.000	1.080	1.003	1.10	1.000				1.000	1.000								
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• 3• BLUME?	14	1.165-93					3,256-92	3.6G=-32	3.526-12	1.456-02	3.135-52	2.195-92	1.945-02	1.422-32	20-11-02	2.37E-33	#					3. 895-02	3.695-32	3.795-72	3.195-12	3.535-12	3.326-02	2.765-32	26-321.	0 0 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	DE-104.	76.104	1.00					1,-3:62	7116-71	D ( 4 L 0 ) 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
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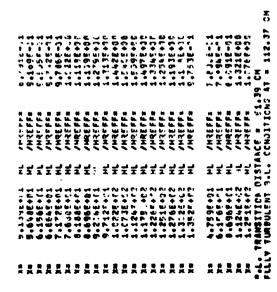
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### RSI GAP HEATING ANALYSIS — II

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#### RSI GAP HEATING ANALYSIS - II

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#### RSI GAP HEATING ANALYSIS - II **VOLUME II**

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## RSI GAP HEATING ANALYSIS - II

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-	RSI GAP	HEATING	ANALYSIS	- [
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## RSI GAP HEATING ANALYSIS - II

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# RSI GAP HEATING ANALYSIS - II

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### RSI GAP HEATING ANALYSIS - II

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Š	2.942-32	2.32E-U2	.367	6.122E-02				2.906-12	1.13		784
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P)	3.545-53	2.065-13	·£ 3·	8.821E-02	3.5946-05	3.403E-05	314.8	3.846-63	1.10		
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### RSI GAP HEATING ANALYSIS - II

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#### RSI GAP HEATING ANALYSIS - II VOLUME II

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FOR PACE B

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	(6/42-5)	6.575-13	6.806-03	9.366-13	1.0 3E-02	6.36E-03	ņ	3.486-03	1-1	1.2 E-02		1.926-02	1,916-02	1.906-02	1.86E-02	1.03E-92	1.90E-02	1.996-02	1.90E-02	1.826-02	1.37E-02	9.615-03	5.46E-03	9.12E-83	6.176-93	4.636-03	3.60E-13	3.96E-03	5.546-03	6.12E-13	4.736-03	2.016-03	1.406-03	
•-	3	314.0	314.0	31.4.3	314.7	7.416	314.3	314.2	_	<u>:</u>	39.0	10.4	11.1	11.2	11.0	e: e1		311.1	311.3	311.3	311.4	311.6	311.0		311.6		312.3	312.6	312.0	313.7	31.3.4	31.3.4	313.3	
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F PREF	(KG/H2-S)	1.(15E-F2	1.482E-12	1.151E-f2	1.1875-12	1.24E-C2	1.261E-02	3-3+62	1.3356-12	4.372E-C2	4.1956-02	7.617E-02	3.5356-62	3.2618-12	2.9846-02	20-3:5402	2.1538-02	1.6616-02	1.39cE-12	1.1936-02	1.0426-02	C * ( T ( E - C )	9.1216-03	9.0875-83	9.324E-[3	9.717E-03	1,0196-02	1.6825-02	1.1515-02	1.187E-02	1.224E-52	1.2616-02	1.298E-02	
HL/HREFF		• 6 32	.62	1000	.574	-688	÷130	•21€	.079	• 25¢	.267	184.	.523	.354	•610	.7 22	.91	157	. 378	476	. 25.	.951	.512	.926	.677	.467	.341	.357	· 4 7 g	.511	392	.229	.116	
_	146/42-51	E - 3, T. )	£ . 40Em : 3	8.515-63	9.535-73	7.985-03	6.446-33	3,465	1.706-13	1.116-12	1.116-72	1.75E-C2	1.756-12	1.746-72	1.735-32	1.686-22	1.748-02	1.826-52 1	1.32E-02	1.675-72 1		e.57E-33	6 . + 2 E - P 3	7.97E-23		4.7CE-03		2.66E-13	F.19E-73	5.756-03	4.556-13	2.745-93	1.42E-03	
ī	(KG/M2-S)	E _ = 5999 * ;	6.765-73	3.305-03	1 4 2	3.425-33	E-#3(# - 2	3.8 95-93	1.368-03	1.1752	1.175-02	1.155-02	1.55=-25	1.845-72	1.225-32	1.775-32	1.935-12	1.526-12	1.936-12	1.765-12	1.316-02	3.135-13	** 675-13	3.415-53	c • 725 - 0 3	£ - 3 + 5 + +	9	3.865-73	5.475-73	0.[65-03	862-23	2.695-13	1.50E-"3	
c.	(A/H2)	£ .+ 3 # £ * *,			E.+4.7.	**345*		2.56 [+3	7.84.E+0	C+37E+3	8-48-4-3	1.36 6434	1.37 6 + 04	1.375+34	1.368024	1.375+14	1.36 5.4.4	1.438+14	10435474	1.715+76	9.77.5+93	. 6. F. F. D. J.	3.1.86.3	0.265+13	26+33200	3.378+93	2.586+03	5.42.463	E	4.565+33	3.5EE+13	2.1 . E+13	1.116+03	
2 {	(;)	ا دن •				5?	4.7		¥.,	7	÷.		4	150	.51	Ξ.	7 :	1	Ξ.	1:	-	-	-i	Ξ:		٠.	;	-	+4 u;	5.	7	٠.	٠	 
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*	?	61.56	56.48	51.39	46.36	46.31	43.77	41.24	19.75	135.24	132.70	30.16	127.63	60* >21	122.56	117.47	112.37	147.31	125.221	97.12	45.26	86.98	61.68	76.97	71.72	£6.44	61.56	56.48	51.39	46.96	46.31	43.77	41.24	36.70
1/0		<b>F</b> :		ij	9	7		5 4								57 1								65	99	£3	99	<b>5</b>	Ļ	1			7.	75
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1 . C.		4	HREFF	25	HOCE	, MREFF	MAEFF	3 2 5	46.6	46 FF	46.0	36.5	HOLEFF	42.2	HREF.	36 FF	REFF	45.5	REFF	44.0	4EF	-	45	
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HEATING UPS	-8736+	.124E+C	377E+0	3+ 3Te 9*	. 8 P. S. T.	1.13	.64.8	.156E	.664E+C	.172F+F	683	+188E+"	1+3969.	.2.4E+F.	.712E+W	*C22E+	.0735.0	.1245+P	.175E+3	.225F+F	.251E+"	.27 6F + C.	-+32:	5.2F+F
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9-L. TPANSITION DISTANIF # 74-7' CM FLLLY TURBULENT 9-L. CINDITIONS AT ##376.09 CM



The control of the		HL/HE		000	:	=			200	300	080					3	į		2	111	ij		.501		. 54.0	546	.526	500	0200		775		.76,	4.4	11 6
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AND	Ç.	#/337		•	•	•	•	-	1.6	2.1	\$ · ·	•										•						•	-	-		•			
The control of the			. 963	100	986	986	786	500	986	.9	716											. 966		996	. 976	.975	.975	.975	9.60		100				
The control of the		HLCC ML/	(/HZ-S)	6.935-02	7.235-02	7.27E-02	7.476-02	A.06E-92	4.376-02	8.69E-02	6.66E-02	24-310-0										366-0		3.785-52	3.495-02	4.085-02	4.13E-02	4 .7 15-02	29-362-9	20-21-5	6 .6 JE-02	30-36-613			
##EN 15 F F F M F F F M F F M F M F M F M F M		_ :	5 🖫										120.7	123.5	6.02	4. 12	122.5	8. 22	23.5	12 3 . 4	123.5	7.221											317.8	317.9	
### FER # 1.12.25   (LVK)   GAP   (ENGT) = 10.05   (LVT)   ENGT  = 10.05   (LV			. 299E-04	7 2 8	10-9	£-04	10-10-14	10-9	- U	10-3	10-3	10-04	90-9	E-04	16-04	# 10 m	-	E-04	10-1	1-3	-0-3¢	40-4	. u-0	10-31	16-04	F-04	36-04	F-34	26-74	10-15	70-16	90-90	36-04	-0-3	5E-04
T	ም ተ ማ	STL	.7:9E-1	46.194.6.4	8.472E-04	8.411E-84	8.5316-04	9.1605-04	9.7335-04	1.7118-03	1.0716-93	1.1025-03	8.216E-04	5.595E-34	3.922E-94	2.876E-84	2.0586-04	1.997E-34	1.94/E-24	1.9706-04	1.8766-94	40-366-5 40-366-6	4.31.5E-04	P.300E-04	4.537E-14	40-30-34	4.7536-34	5.41 36-34	6.7545-34	40 - M - C - C - C - C - C - C - C - C - C	40-140-1	10-30-5-7	3.775 6-24	3.53AE-34	2.518E-74
##ES 3.5 F* HHT #ETT (L2), 2.5. SLUKER INVERS 14 # 1.16.2 F* 1.2	1 (2H/M)	F MREF	(KG/M2-S)	377.6	1425-02	50-3645°	1.76E-02	1 A C E E E E E E	164E-02	195E-52	3196-02	.065E-02	73-35-67	5468-02	3948-02	3716-02	21-11104	593E-C2	. (34E-[2	£96E-02	727E-82	.75 es-62	1 195-62	3876-02	154E-C2	771717	1926-02	16cE-[2	.73E-52	. 935-52	30124	17 4 E E E C C	7315-02	1305-02	
### ##################################	100000 10000 10000 10000 10000 10000 10000	L/HREF	.746	:	.375	206.	)c6.	26.93	624	263	655	190		. 227	.386	7.36	168	. 3F3	12.5	689	.921	.837	150	. t. 35.	• 471	, F + 7	563	.7.2	1.41	996	5 4 5 4	4.00	75.	206	738.
THE		ļ.	419E-02		6.756-32	6.796-02	F.38E-02	7.12E-12.1	7.615-32 1	4.12E-02 2	8.346-02 2	9.35E-32 3	/ . C. 4 E = . Z . 3	4.736-02 3	1.15E-"2 2	2.25E-C2 1	1.555-52	1.606-02 1	1.566-02 1	1.566-32	1.516-02	1.395-32	3.23E-"2	3-156-72	3.645-32	3.325.0	1.015-02	** 35E - 12	4.366-02	5.3(E-12.	7 - 356 - 1	20.	1036612	2.366.2	20-106-02
THE NAME   THE PROPERTY   THE PROP		ĭ	KG/H2-		0.03C-72	7.165-72	-372-92	7.735-12	31.14.14	1.588-12	3.495-72	9.535-32	7.655-02	1.595-32	3,335-32	2.38E-02	1.745-32	1.695-72	1.655-32	1.67:-32	1.595-02	1.475-72	3.41E-12	3.695-02	3.645-02	4	3.3E-32	20-265-4	3.136-72	5.69E-02	21-38:	F = 25-92	71 - 145	3, 155-32	2.14.7.47
NAME	(132), (K) (1/K) (1/K) (1/K) (1/K) (1/K) (1/K)		M/ W2)		405+34	175+54	27.6+34	5 4 E + 3 C	40.44.00	125+34	140+E	4:439	466446	575+34	375494	775+34	2 E 4 3 4 2 4 2 4 2 4 2 4 2 4 2 4 2 4 2 4 2	216+34	175+04	106674	136+34	45434	30+400	4 1 5 + 9 4	*0+3		30000	7.4362	7.+30.	41+32 )	40.0	1 4 5 4 5 1	46434	105+34	1000
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	TTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTT		(64)	32.70	30.16	25.79	22.56	17.47	12.37	02.23	97.12											39.73	35.24	33.16	27.63	25.79	95.52		27.31	12.20	51.15				
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	AL/HE		1.250	1.513	1.521	1.520	1.067	.795	.307	,	.212	.210	. 36.	. 362	.371	.372	.366	. 353	. 362	1640		.511	200	-216	ER.	0 P	. 544	166	762-1	1.132	121.1	201	386	.110	
96	HLCC/HREF									1	• 174		100.	. 322	175.	. 362	. 199	. 461	.595	1991	1.263	1.651													
PAGE	HL/M.CC H										.927		.050	. 960	196.	196.	.963	.959	- 962	979	.974	.976													
	HLCC HL	G/M2-5)									1.556-62		2 • 5 2E - 02	2.62E-32	2.70E-02	2,796-6.	2.636-02	2.69E-82	3.0.8	3.496-02	4.166-02	4.376-82													
	-	ŝ	310.2	316.3	317.1	317.9	317.8	317.7	317.6											31.3.0		315.5	312.8	311.7	312.1	312.6	313.1	313.6	314.2	314.7	316.0	315.6	318.5	315.4	
	511		2.3616-54	3.1826-04	2.676E-04	2.917 6-04	2.0336-04	1.3146-34	5.4536-05		1.661E-34	1.6556-04	2.676E-04	2.81+5-44	2.907E-34	3.7026-04	3.0426-04	3.0536-64	3.248 6-04	3.785E-04	4.5246-04	4.762E-04	4.176E-04	2.212E-04	1.8466-04	1.2756-04	1.5056-04	2-1616-04	2.4386-04	2.1496-84	2.077 6-04	1.330 6-04	5.5696-05	2.1966-05	
1973	STL										1.6916-04	1 7476-34					3.2126-34				4.7766-74	5.028E-04	** 31.38-04	2.335E-94	1.9496-04	1.3458-04	1.674E-04	2.282E-94	2.573E-0+	2.263E-34	2.1946-54	1.412E-34	\$ . 9: 2E-0 \$	2.2146-09	
-Or ( +8)	HREF	(KG/H2-S)				1.t 336-62														4.55E-C2									1.4945-02		.6336-62	. (658-02	. 696 E-02	.7276-02	
dyn Ise	HL/HREFF		1.01	848.1	10018	1.54	156.1		.2E3 1											.326 4								_	1.462 1	-	~	*1	**	1 6.13	
STUMES, IN-LINE	ī	(K3/k2-S)	2:-3110	20016-32	2	2. 396-12	1.726-12	1.116-72	4 .0 2E- " 3		1.365-72	1.468-12	2.27E-02	2.35E-f.2	2.176-12	20-366-5	2.586-12	2.306.2	2-156-02	3.216-12				1.988-72	1.57E-62	1.086-32		1.83E-02	~	1,516-92		1.13E-12	L.74E-C3	1.786-03	
rese atumise						2.525-02		1.182-12	E - 180											3, 375-02											1.665-12	1.20=:12	F 1E-33	1.685-73	
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## RSI GAP HEATING ANALYSIS - II

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		. 639		1.170 1								74.							565	175	940.			610	.267	.23	6109	***	21012	
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<b>.</b>	HLIMCC	4	_					_											÷-	: :	÷			•		. ∾	~:	<u>~ ~</u>	<u>, , , , , , , , , , , , , , , , , , , </u>	4 9
	HCC #	1.406-02	1.56E-9	1.95E-02	2.12E-8		1-136-1	\$-70E-0	7.426-9	!		1.20E-02	3.235	2.06E-0	2.47E-0	2.40E-0	- 3K - 7		4.40E-09	2.496-	6.516-3			6.646.A	7.23F-	7.196-	7.07E-	6.67E-	3.51E-0	
	-ŝ	326.1	329.6	327.6	325.2	323.4	320.9	310.9	317.07			325 . 1	1.026	32+16	323.2	322.7	361.		317.8	316.3	315.8			461	3.28	323.0	322.5	321.9	320.0	
	TTS	1.5518-04	.7376-04	2.1638-04	. 1936-04	.2306-14	.2516-04	. 3336-05	. C. E. C.			1,3266-34	1.3006-04	2.292E-04	2.7416-84	2.6656-64	2.6538-04		1.1616-04	2.7686-25	7.2336-06			10.75.01	10-111-01	7.9856-04	7.854E-04	7.6346-64	E.493E-04	20163406
	STL	1.6406-84	1.8375-94	2.2876-04	F.467E-04	2.357E-04	1.322E-54	5.492E-05	2.8386-35			1.4.46-74							1-1536-74	. E = 0.5	90-3			700	4, 17, 18, 18, 18, 18, 18, 18, 18, 18, 18, 18	40-110-4	. 3f 2E-34	9236-34	6.820E-04	./ 31E-34
	HREF (KG/H2-S)	E-02 1		1.664E-(2 2										23E-82					-25E-12					_	_				2208-52	
<b>, z</b>		1.665	•	** *		•						7			: =	-	-		-					•	•		Ň	Ň	ď.	Ň
100 100 100 100 100 100 100 100 100 100	HL/HREFF	. 539	946.	1.170	1.272	1.206	1.0333	. 342	. 145			.8+2	99	1.167	1.731	1.683	1.575		9	175	7.0			;	2170	3.243	3.155	3.094	2.515	2 . 197
1	HT (KG/H2-S)	1.32E-t2		1.846-02	Ġ	٠,	٠.	÷	0	•		1.136-32	1.166-02	1.57E-02	2.336-02	2.276-02	2.265-72		9.37E-33	3.245-1.3	6.165-04					868-7	696-0	305	4 - 4 O E - 5 2	.625-3
1 4 4 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	PL (KG/M2-S)	1.488-12		955-32										1.665-02					.902-13		? .			(	9,0	7 5	32	87E	7.817-72	20
14/42) 13/45) 13/46) 14/46/12-5)	(3/H)	9.A2E+33		1.346414		396.	357	.98E	6.95			.2 8 E	, F.	1.15 6 4 36	1	. F. 7.	•EEE		.936+)	765.4						10	916	8	1,47,5434	
	22	e	. t.	00.0		• 58	 	6€	1.16	1.65	2.0.0		~	ن د د د	•	-	۲. ۹ ۱۳. ۱		÷.	٠.	: :		5.19		•			•	<b>W</b>	
	<b>* F</b> U	1.52	1.15	٤.		. 00	0 °	3.03		, L		1.32	1.9	.51		66.0	5		9.39	F. 6		1.31	(.19	.75				ξ.		
TTT FT FT FT HACHE RMC VEL FAM/HT HCC	×£	47.59	47.59	47.99	67.59 67.69	47.59	47.59	47.59	47.59	47.59	47.59	61.56		6.		. *	F: 1		£1.96	*		::	1.5	95.59	96.96	16.96	96.	36	ž	4
<del></del> -	27.0	P) (	2.2			12	۲ <u>۱</u>	, w'	4	7 2	5.2		Ş	26	9 6	=	21	2	512	2:		5	ວຂະ	¥	7.5	a' c			Ξ.	33.5



EF 11.116		727					•	•	•								.131										1990						
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5 FT HWT TEST (1%2), C.2. 91 8 1.13746+3(K) # 1.675966+06(K) M2) # 1.27436+06(J) KG) Q = 9.121496+06 R 5.130

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	-	_ '	316.6	317.4	317.6	317.9	317.8	317.9	316.4	318.4	310.5	31.8.8	319.6	319.5	318.4	313.4		6.61E	S • 829	350.0	3.026	350	1.076	319.0	319.0		326.1	124.1	723.1	321.6	, 12t	323.1	•			321.6	321.7	35, 3	320.7	34 3 . 8
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2	ī	(KG/H2-S)	3.615-02	3.12E-22	2.935-02	2.62E-32	2.406-12	1.996-12	1.605-92	1.335-52	1.136-72	9.536-03	4.682-73	7.32E-93	7.636-93	7.61E-03	# - 22E-43	B-00E-03	3.35-33	9.515-93	9.97E-73		26-189-1	1.025-92	1.105-72		5.535-13					2.15E-03				4.56E-23	3.345-34	7.62E+#3	5.135-33	2.79E-F3
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399 86.				_	2.236-03	2.12E-43	152.	9.67EE-03	5.429E-05	5.142E-05	310.1	2.236-13	1.340	122	386
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# RSI GAP HEATING ANALYSIS - II

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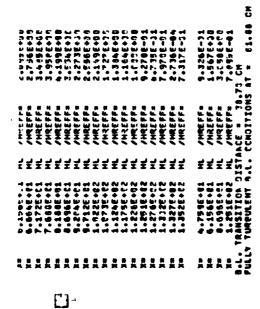
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MCDONNELL DOĞGLAS ASTRONAUTICS COMPANY . EAST



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# 1-1202000   1			2.11 (K) E+11(K)	•		KE IN TINE ASI	451 GEP 1.5G2 (CH)	CAS DANA C	197.3				PAGE	E 11 3	
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19. 3LUME 4.	14	3.050.00	1.47:-12		1.150-75	3.442-13	1.955-02	22140	5.12=-12	26-36-12	3.515-12	4.21E-32	3-135-72	1.805-72	1.195-72	3.362-03	2.t. £-03	1.993-53	2.49=-13	1.402-73	20-246-5	3.535-02	2.115-32	26-362-	3.865-02	2,-363.	36 - 100 + 7	1.195.2	1000	F ( ) ( ) ( ) ( )		4,725	3.45 43	1, 16 - 17	*****
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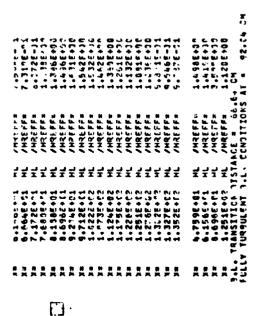
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## RSI GAP HEATING ANALYSIS - II

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## RSI GAP HEATING ANALYSIS - II

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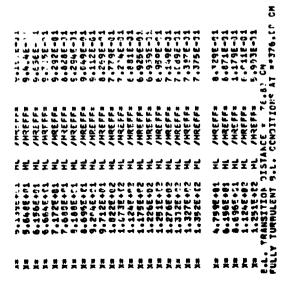
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## RSI GAP HEATING ANALYSIS - II

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	HCC	(S-24/)	4.95E-03	1.126-09		1.076-99	2.576-13	2.362-92	2.096-02	1.95E-82	1.736-12	1.046-02	5.946-03	1.35E-03		7.09E-02	6.985-02	6.406-02	5.196-02	5.146-12	20-364.4	2.986-52	1.876-62	4.196-13	5.57E-14	6.766-82	6.505-02	6.27E-12	9.57E-02	5.046-02	28-38/**	20-14-4-5	2 4 3 E - 5 A	1.26E-83					
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	STT	. 5.375 -A.S.	5.6228-05	1.2666-17		1.2176-07	2.9176-05	2.6798-64	2.376E-04	2.2196-84	1.9606-04	1.1776-04	6.751E-05	1.5306-05		8.(566-34																		1.4356-05					
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IN-LINE	H	6.29E-13	**69E-03	1.765-35		1.025-05	2.435-33	20-342-	1.986-02	1.858-32	1.04E-0.2	9.825-73	5.63E-R3	1.266-63		72E-12	20-329	37E-52	F.586-32	**87E-32	4.26E-02	2.32E-12	1.776-92	PG-349.7	5.285-34	D.40E-02	6.166-32	20-346-3	5.28E-12	20-30/0	27-164.1	3 245 -02	A . 205.11	1.20E-03					
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(11.2), C.	٠,	2-18-5-7	3.672+03	7.4336.7		7.6~E+*C	4.36.43	1-3-7		446+1		44.7		. 15 + 1		*21E+J#	.16 C+14	.74E+74	.3EF+94	3.015+74	.33E+14	*51E+##	30E+36E	.65 . 433	~			£	3					2E+12		# H	12	1 1 1	# L
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## RSI GAP HEATING ANALYSIS - II

H. H. H. H. H. H. H. REFF ST. ST. ST. T H. LC H. L. M. C. M.	AMES 3.5 FT HWT TYST (142), C.3. BLUMPR, IN-LINE
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2-35E-73 .116 2.10E-02 2.977E-35 2.814E-85 348.8 4.84E-83 1.888 .118 2.10E-02 3.116 2.814E-85 348.8 4.84E-83 1.888 .118 2.10E-02 2.84E-85 31.87 2.95E-72 1.82E 2.118 2.12 2.12 2.13 2.13 2.13 2.13 2.13 2.13	(KG/H
2.35E-73 .116 2.106E-02 2.977E-35 2.614E-85 348.8 2.48E-82 1.226 2.106E-02 3.17E-04 2.952E-14 315.7 2.59EE-02 1.097 2.106E-02 2.48E-04 315.7 2.59EE-04 315.7 2.24EE-02 1.097 2.106E-02 2.48E-04 2.99EE-04 312.7 2.88E-02 1.098 2.99EE-02 2.48E-02 2.48E-02 1.09E-04 316.89 2.48E-02 1.098 2.48E-02 1.09E-04 1.196FE-04 316.89 2.48E-02 1.098 2.48E-02 1.09E-04 1.196FE-04 313.3 7.43E-02 1.098 2.48E-02 1.09E-04 1.196FE-04 313.3 7.43E-02 1.098 2.48E-02 1.09E-02 1.09E-04 1.196FE-04 313.3 7.43E-02 1.098 2.48E-02 1.09E-02 1.09E-04 1.196FE-04 313.3 7.43E-02 1.098 2.48E-02 1.099 2.99E-02 1.09E-03 1.09E-04 1.196FE-04 313.3 7.43E-02 1.098 2.48E-02 1.099 2.99E-02 1.09E-04 1.196FE-04 313.3 7.43E-02 1.098 2.48E-02 1.099 2.09E-02 1.09E-04 1.196FE-04 313.3 7.43E-02 1.098 2.09	4. 84E
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2.35E-73 .116 2.106E-02 2.977E-75 2.614E-85 340.0 2.45E-83 1.000 1.225 2.45E-12 1.22E 2.116E-02 2.45E-70 1.777 2.116E-02 2.45E-70 1.777 2.116E-02 2.456E-94 31.59 2.977E-70 1.777 2.116E-02 2.456E-94 31.59 2.877E-94 31.59 2.877E-92 1.000 1.225 1.000 1.225 1.046E-02 2.456E-94 31.59 2.877E-92 1.000 1.00	
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5.49E.03 .273 2.12E.0E.02 6.990E.09 6.90E.09 307.9 9.54E.06 1.000 1.009 0.009	1.055-92
9.14E-74 0.045 2.42E-02 1.149E-09 1.009E-04 315.3 7-13E-02 1.000 1.189 6.62E-02 1.160 2.189 1.189 6.62E-02 1.160 2.189 1.189 6.62E-02 1.160 2.189 1.189 6.62E-02 1.160 2.189 1	5.79E-03
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6.755-C2 1.165 9.094E-D2 6.535E-D4 6.104E-D4 313.3 7.13E-D2 1.000 1.109 5.00E-D2 1.166 5.092E-D2 1.166 5.090E-D2 1.000 1	
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\$ 958E-02 1005 \$ 936E-02 5.72E-04 5.65E-04 33.5 5.65E-02 1000 0935 5.35E-02 0.935 5.99E-02 5.	6.985-72
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\$408E-02 6.80 5.908E-02 6.908E-04 2.937E-04 312.0 7.958E-02 1.808 6.427  2.42E-02 6.427 5.908E-02 3.058E-04 1.6582E-04 312.0 7.958E-02 1.808 6.427  2.42E-02 6.427 5.908E-02 1.758E-04 1.6582E-04 313.0 7.8082E-03 1.808 6.427  2.42E-02 6.427 7.727E-02 1.758E-04 1.6582E-04 313.0 7.808 6.428  2.42E-02 6.427 7.727E-02 2.773E-04 7.6597E-04 313.0 6.582E-03 1.808 6.428  2.42E-02 6.77 7.727E-02 7.835E-14 7.621E-14 313.0 6.56E-02 1.808 6.428  2.42E-02 6.677 7.727E-02 7.835E-14 7.621E-14 313.0 6.56E-02 1.808 6.63  4.45E-02 6.677 7.727E-02 6.357E-04 313.0 6.56E-02 1.808 6.63  2.45E-02 6.677 7.727E-02 6.357E-04 313.0 6.56E-02 1.808 6.63  2.45E-02 6.677 7.727E-02 6.357E-04 313.0 6.56E-02 1.808 6.63  2.45E-02 6.677 7.776E-02 6.357E-04 5.357E-04 313.0 6.56E-02 1.808 6.63  2.45E-02 6.777 7.776E-02 6.355E-04 5.357E-04 313.0 6.56E-02 1.808 6.63  2.45E-03 7.776E-02 2.531E-04 2.135E-04 31.0 1.808E-03 1.908 6.047  2.45E-03 7.776E-02 6.355E-04 6.356E-05 309.7 3.64E-03 1.908 6.047  2.45E-03 7.776E-02 6.355E-04 31.808 6.808 6.047  2.45E-03 7.776E-02 6.355E-04 31.808 6.808 6.047  2.45E-03 7.776E-02 6.355E-04 31.808 6.808 6.048  2.45E-03 7.776E-02 6.355E-04 31.808 6.808  2.45E-03 7.776E-02 6.855E-04 31.808  2.45E-03 7.776E-03 6.856E-04 31.808  2.45E-03 7.776E-03 6.8	F. 69E-72
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## RSI GAP HEATING ANALYSIS - II

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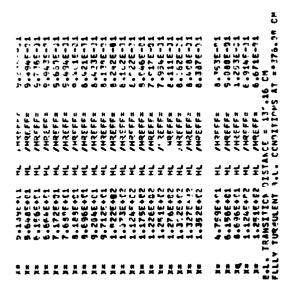


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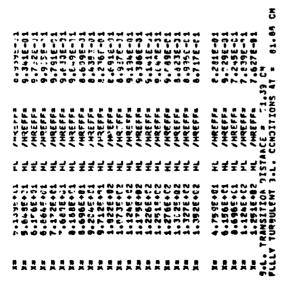
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## RSI GAP HEATING ANALYSIS - II

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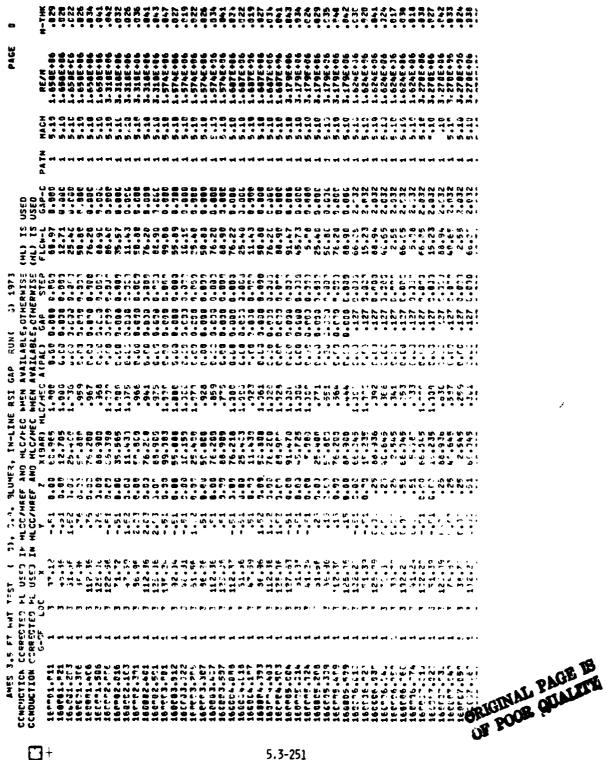
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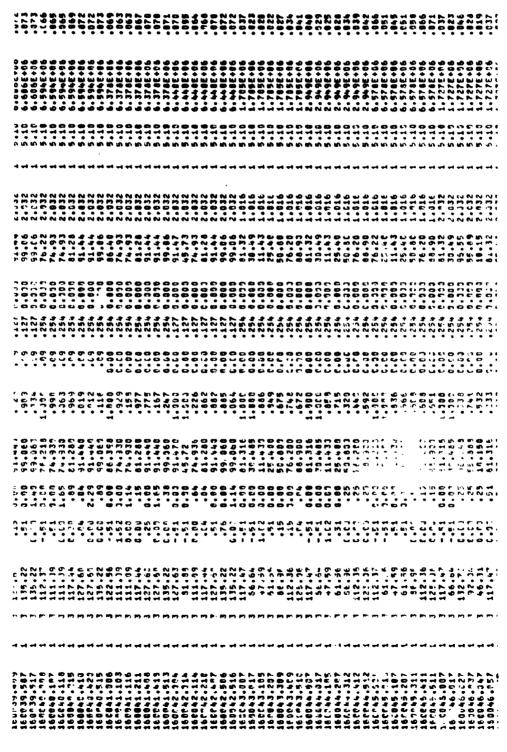
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## RSI GAP HEATING ANALYSIS - II

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## RSI GAP HEATING ANALYSIS - II

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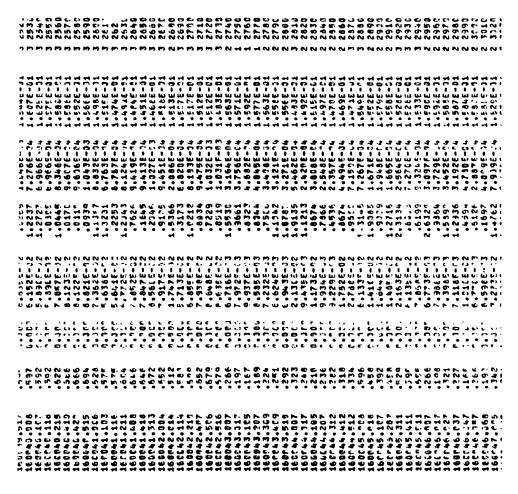


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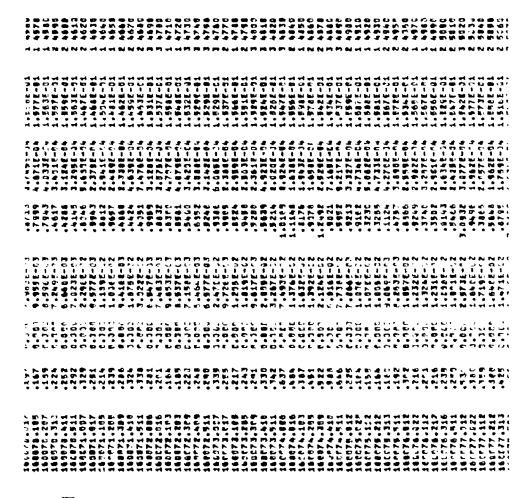
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RSI GAP HEATING ALLYSIS - II

#### 6.0 NASA/Larc, 8 FOOT HIST TESTS OF LARGE GAP PANEL

Cap heating tests were performed in the LaRC 8 Foot High Temperature Structure Tunnel (HTST) to obtain heating data on a large gap panel in the presence of a turbulent boundary layer. The test program at LaRC was under the direction of I. Weinstien. The test panel consisted of eleven LI 900 silica tiles with an interchangeable thin skin metallic center tile. Testing was planned for both the center LI 900 tile and the center metallic tile, but time permitted testing only of the metallic tile. The panel size was 46 x 46 x 6.5 cm. Both the LI 900 and the metallic tiles were heavily instrumented as discussed in Section 6.1. The RSI panel was mounted in a large test sled for free stream testing and permitted variation of angle of attack relative to the tile array. The panel was tested in both the in-line and staggered tile configurations.

The test matrix for the 8 Foot HTST program is summarized in Figure 6.0-1. Five gap settings were employed (0, 0.10, 0.18, 0.30, and 0.41 cm) with the tile thickness of 6.35 cm. Step heights investigated were 0 and  $\pm$ 0.254 cm. Tests were run at Reynolds number per meter of 1.9 x  $\pm$ 10 and 4.8 x  $\pm$ 10, while the test sled angle of attack was varied from 0 to 15 degrees.

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# CONFIGURATIONS FOOT HTST ∞ TESTS IN TEST CONDITIONS AND MODEL HEATING GAP

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	Re/m	2.069x10 <sup>6</sup>	2.001	2.001	4.823	4.692	1.969	2.1	2.001	4.692	2.001	2.001	1.969	1.903	2.001	1.870	2.034	2.001	2.034	1.969	1.870	4.692
	MACH NO.	6.35	6.54	6.6	6.50	6.65	6.87	9.60	6.58	6.64	6.65	6,65	6.76	6.90	6.70	7.00	92.9	6.21	9.60	9.60	6.70	6.45
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1014	OK OK	1533	1656	1700	1733	1822	1833	1639	1667	1831	1706	1711	1772	1844	1722	1886	1767	1492	1689	1694	1722	1719
NOMINAL	o DEG.	7.34	-0.14	15.15	7.63	-0.10	7.64	7.40	7.49	0.14	7.56	7.53	7.66	-0.15	14.96	7.63	7.49	7.53	7.30	7.70	0.10	0.08
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### RSI GAP HEATING ANALYSIS - II

6.1 Model Description - A large gap panel was fabricated for performing heating tests in the presence of a turbulent boundary layer. The same test panel was to be used in both the HTST and the AFFDL 50 MW Arc Turrel Tests. The panel was originally scheduled for testing at AFFDL but was switched to the LaRC HTST due to fabrication difficulties with the test fixture by the vendor. The 50 MW tests were intended to determine the effects of higher enthalpy on the heating in a field of RSI gaps, and would have also provided a comparison of arc and wind tunnel gap heating data. The AFFDL test program was subsequently cancelled.

The test panel as shown in Figure 6.1-1 consisted of eleven LI 900 silica tiles with an interchangeable thin skin metallic center tile. Testing was planned for both the center LI 900 tile and the center metallic tile, but time permitted testing only of the metallic tile. The panel size was 46 x 46 x 6.5 cm.

Both the LI 900 and the metallic tiles were heavily instrumented with the thermocouple locations for the thin wall metallic center tile shown in Figure 6.1-2. The RSI panel was mounted in a large test sled for free stream testing and permitted variation of angle of attack relative to the tile array. The panel was tested in both the in-line and staggered tile configurations. Figure 6.1-3 shows the flow orientation for the RSI tile array. Tile numbers affixed to the tiles are also shown. Gaps between the tiles were adjustable to study the effects of gap width, and shims were used under the tiles to study the effects of step heights. A companion plate that fitted into the same opening as the test panel was used for calibration purposes.

The following drawings (Figures 6.1-4 thru 6.1-10) were prepared to define the various detail parts and assemblies:

- a. 70J037004 50 MW Arc Tunnel Plasma Wedge/RSI Tile Interface
- b. 70J037005 Study Enclosure of Fwd End in 50 MW Plasma Wedge Test Compartment
- c. 70T037039 RSI/Sponge Assy 50 MW Plasma Wedge
- d. 701939740 Tile Assy 50 MW Plasma Wedge
- e. 70T030741 Shim & Spacers 50 MW Arc Tunnel Plasma Wedge
- f. 70T037042 Support Assy 50 MW Plasma Wedge
- g. 70T037043 Installation Assy 50 MW Arc Plasma Wedge Sheets 1 and 2

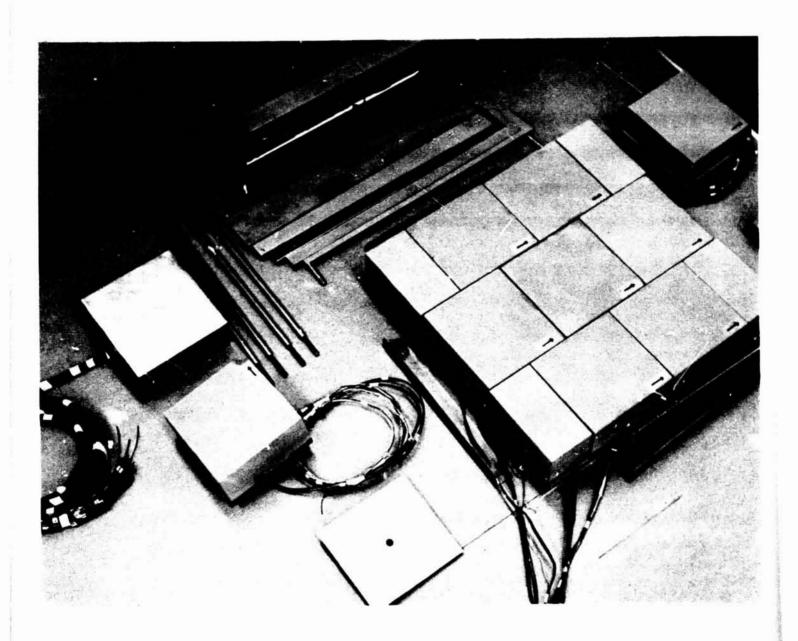
Thermocouple locations were confirmed and/or determined with the use of x-rays of the instrumented tiles. When x-rays were used, the effects of parallax were accounted for in the measurement. The x-rays are documented in Figures 6.1-11 thru 6.1-19.

RSI GAP HEATING ANALYSIS - II

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#### 46x46 CM RSI GAP HEATING EVALUATION PANEL MINIMUM GAP SETTING

LaRC 8 - FOOT HTST TESTS





### 46x46 CM RSI GAP HEATING EVALUATION PANEL MAXIMUM GAP SETTING

LaRC 8 - FOOT HTST TESTS

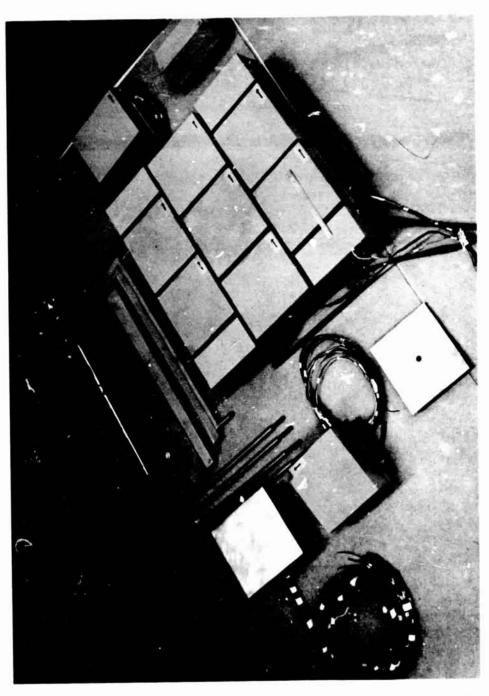
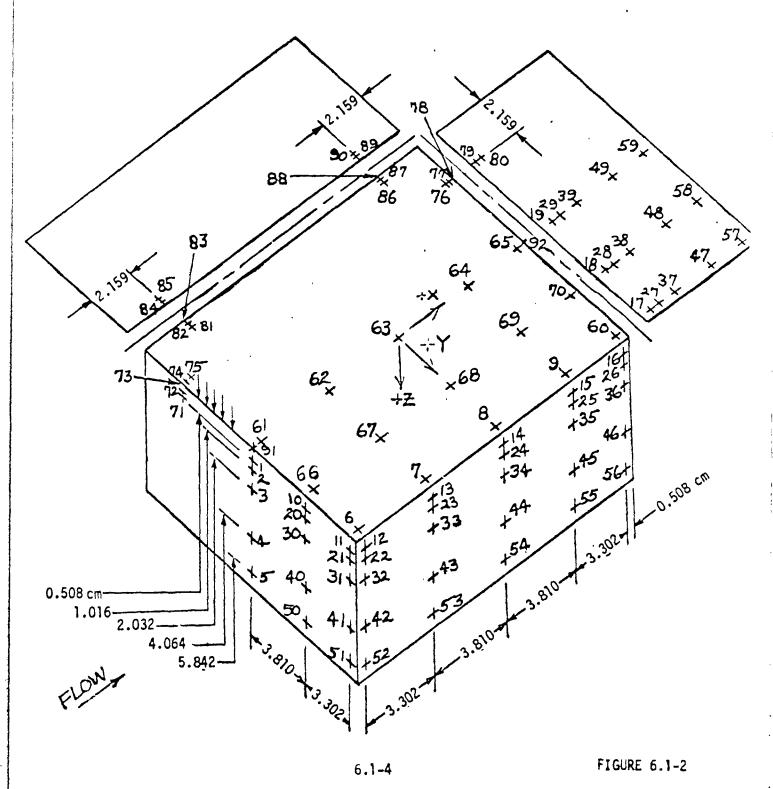


FIGURE 6.1-1 CONC.

REPORT MDC E1248 JSC U9651

### THERMOCOUPLE LOCATIONS ON THIN WALL METALLIC CENTER TILE



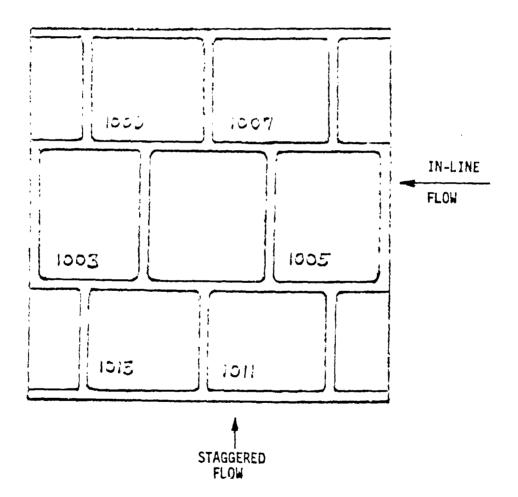
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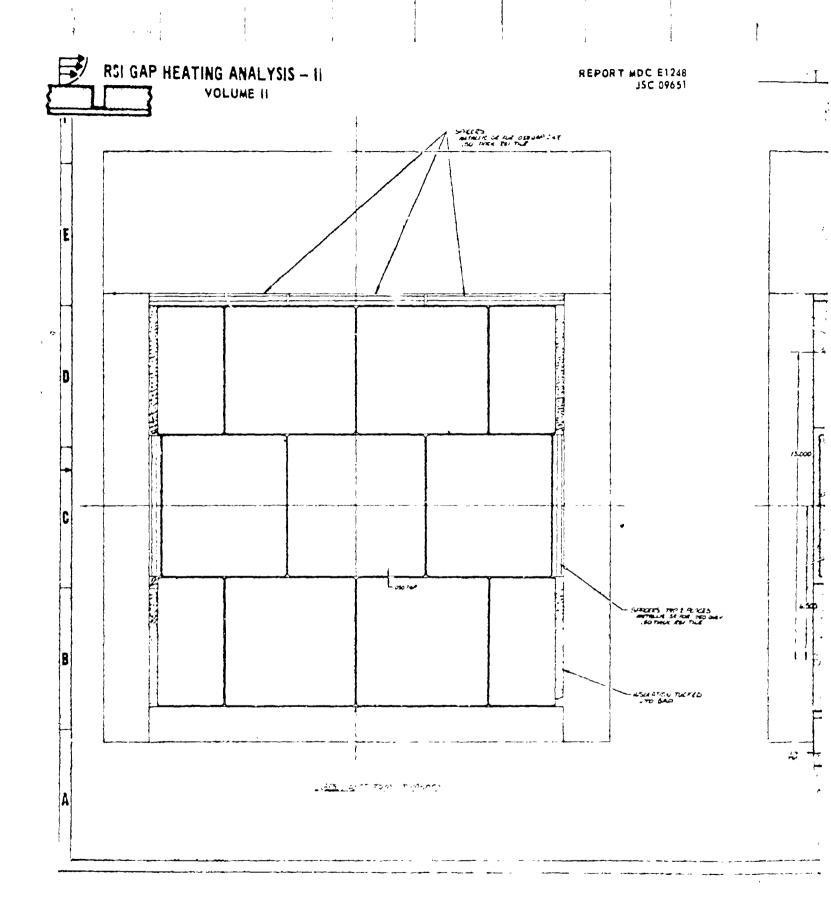


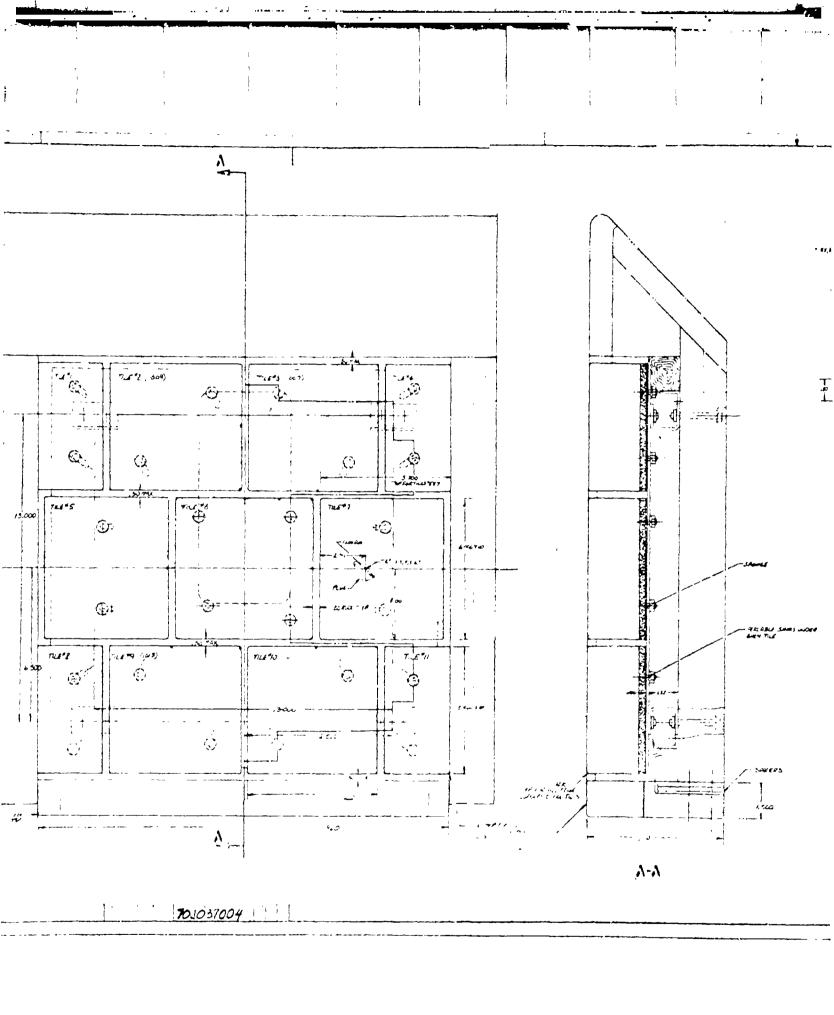
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## FLOW ORIENTATION FOR TESTS OF RSI TILE ARRAY

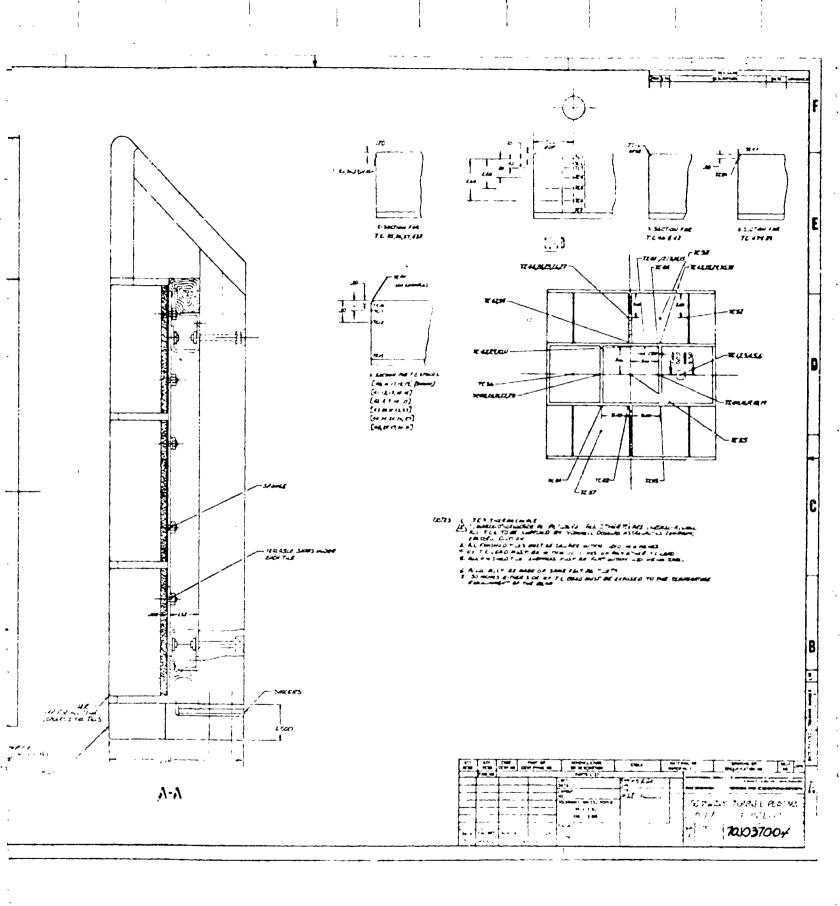
(TILE NUMBERS ARE SHOWN ON SKETCH.)



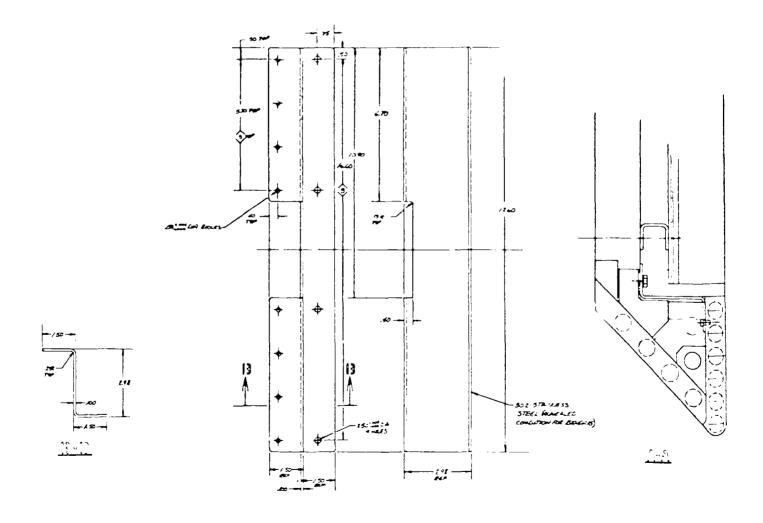




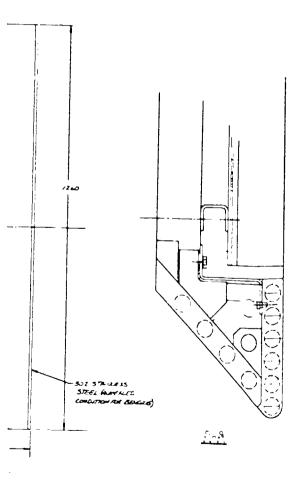
OLDOUT FRAME







FOLDOUT FRAME



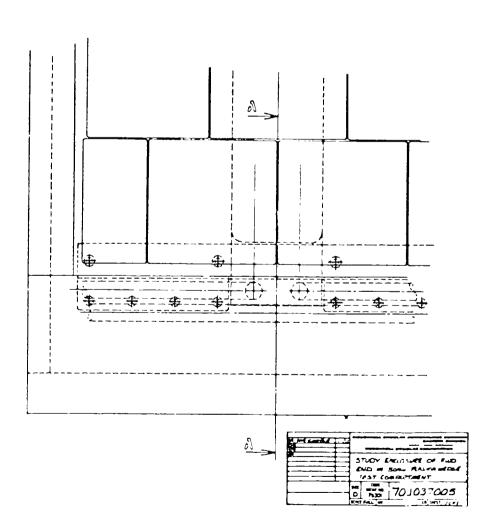
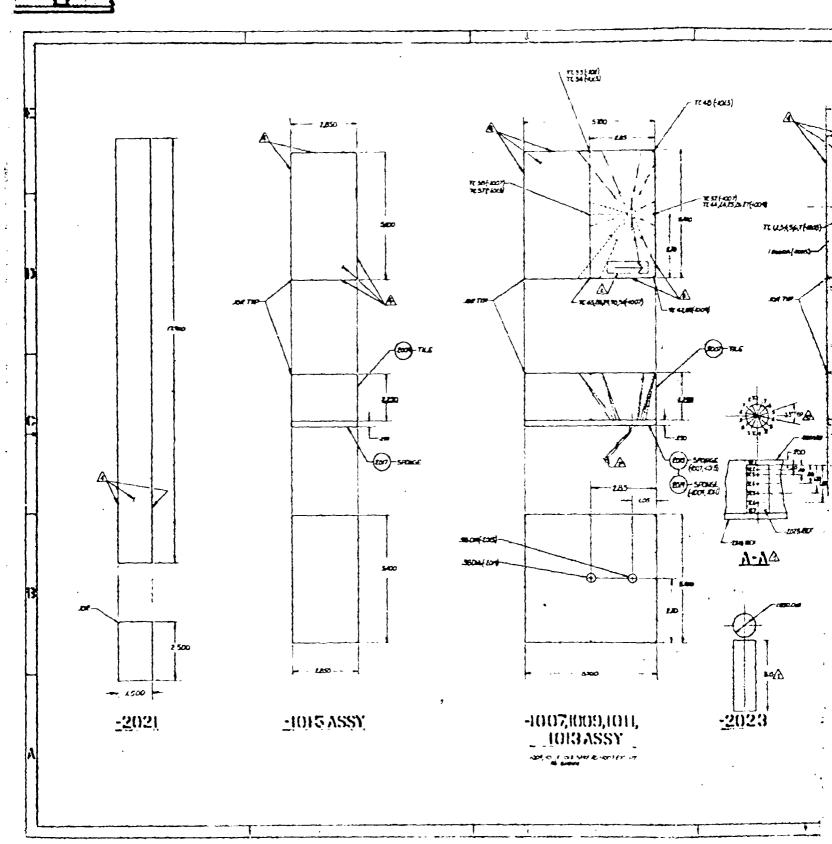
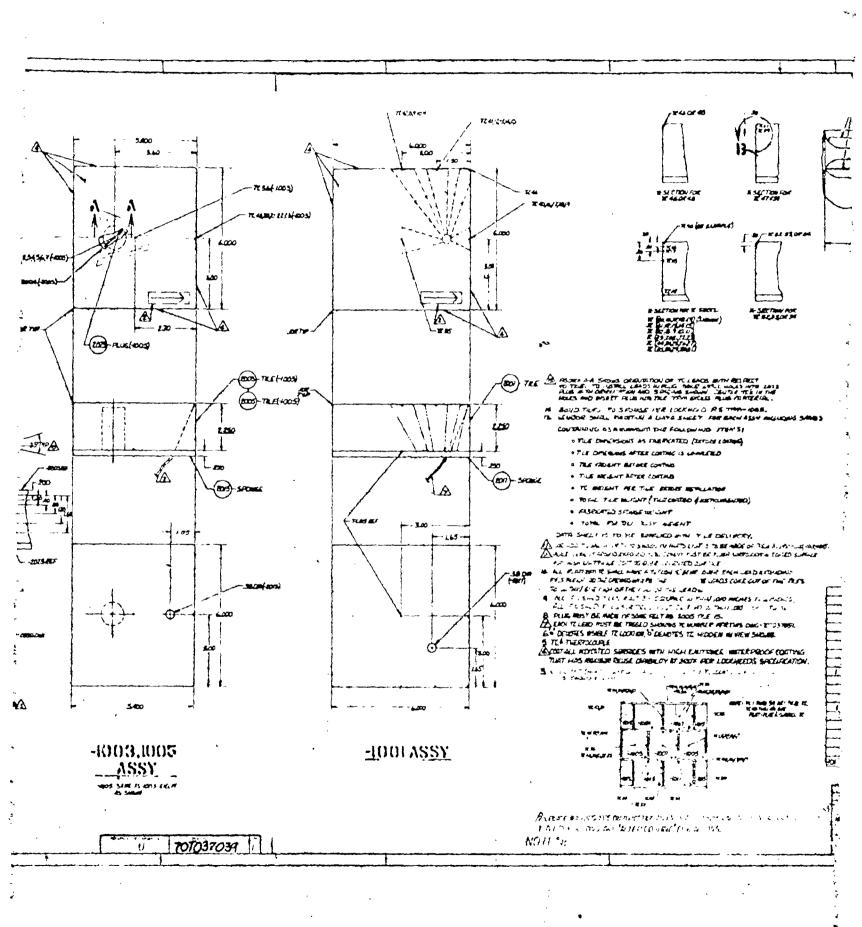


FIGURE 6.1-5

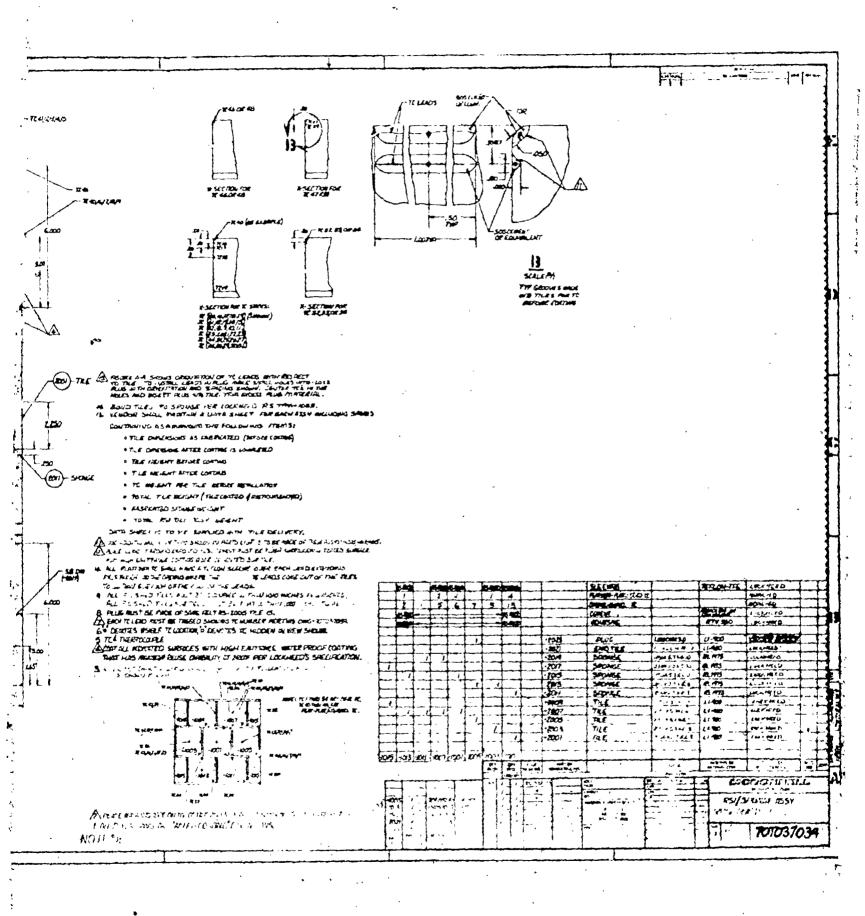


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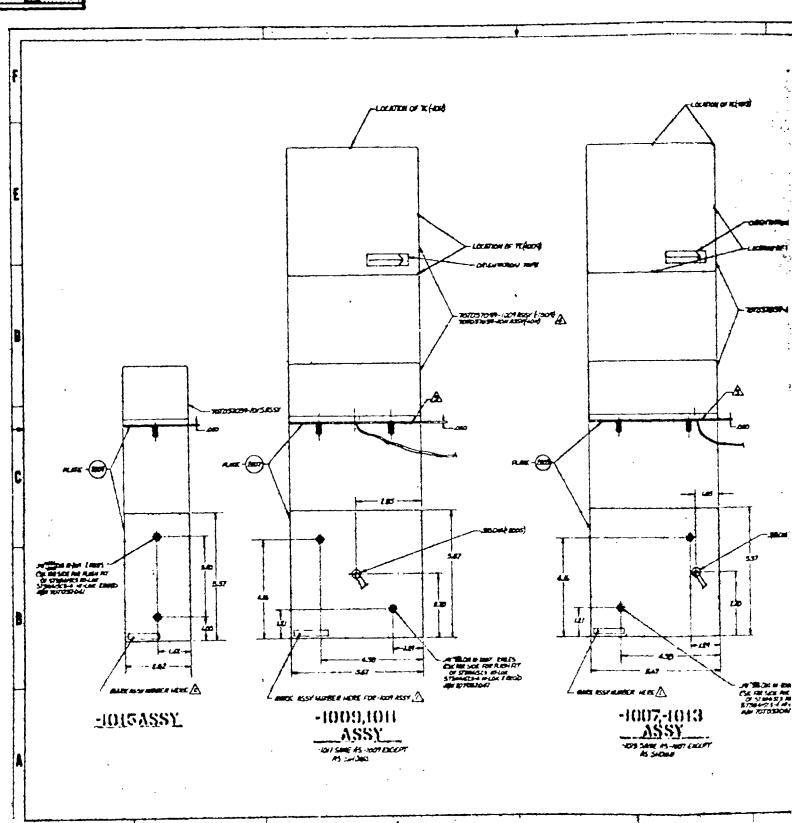
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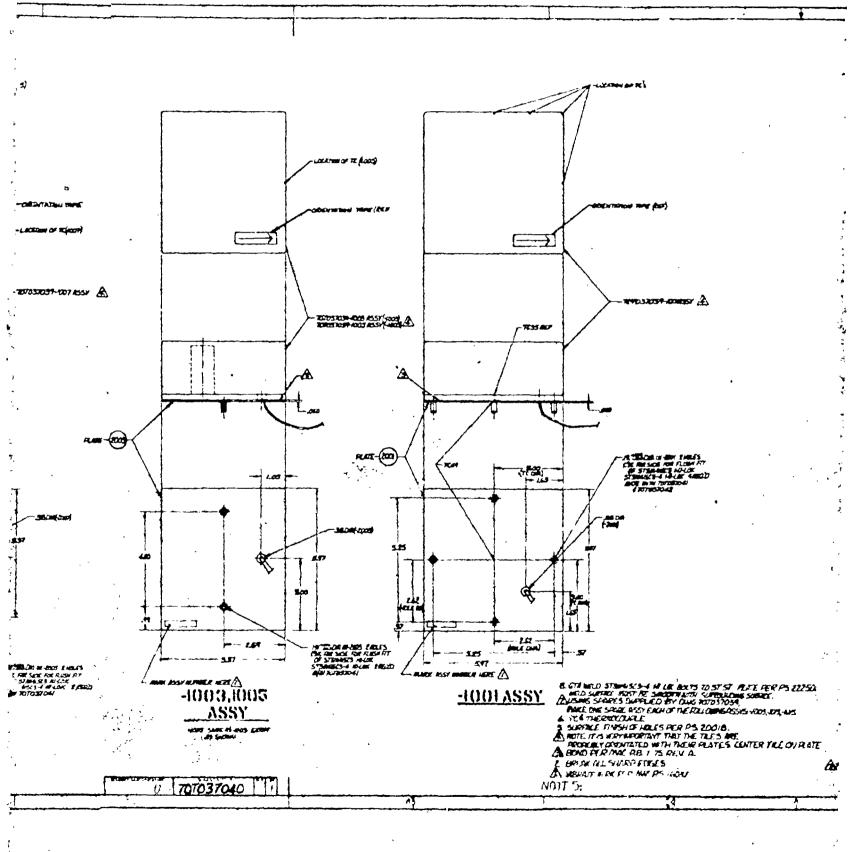


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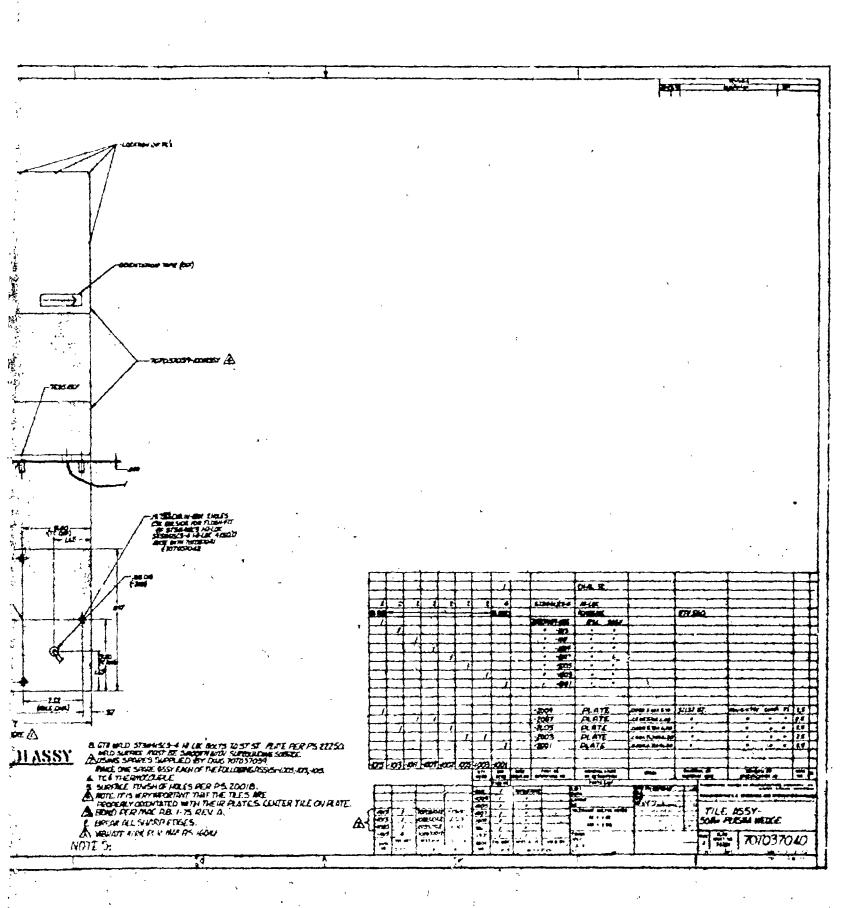


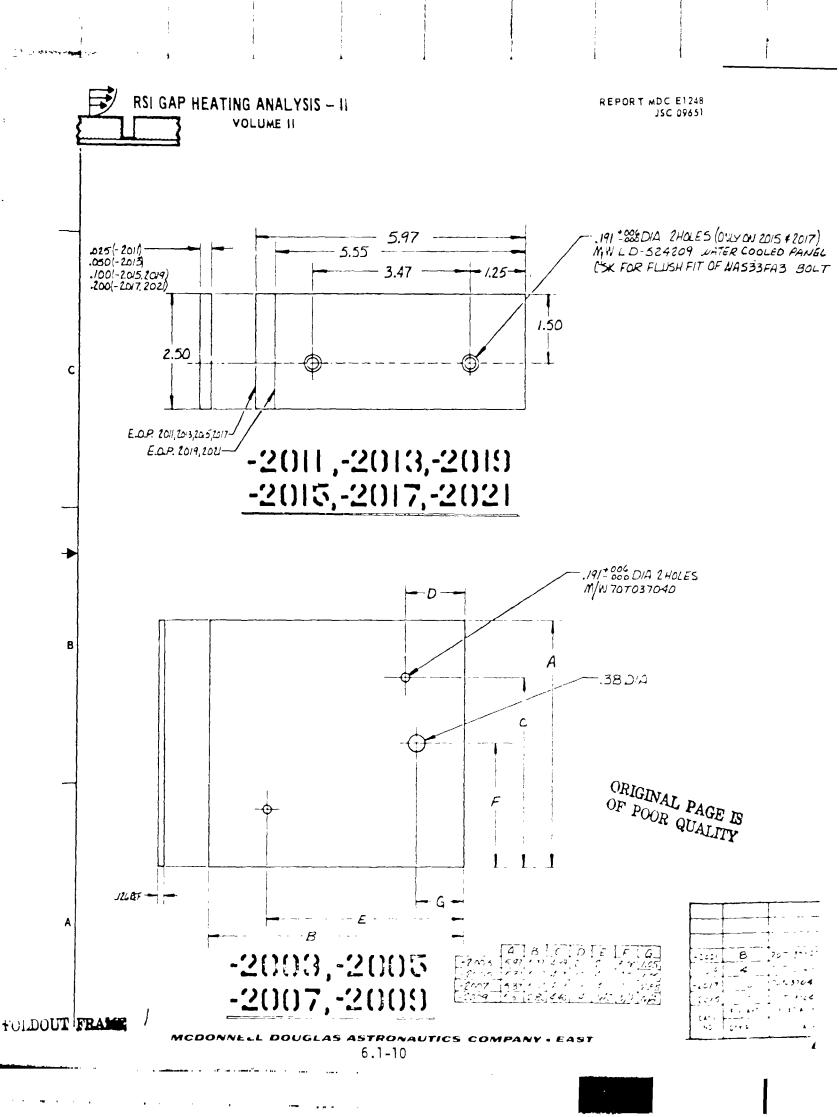


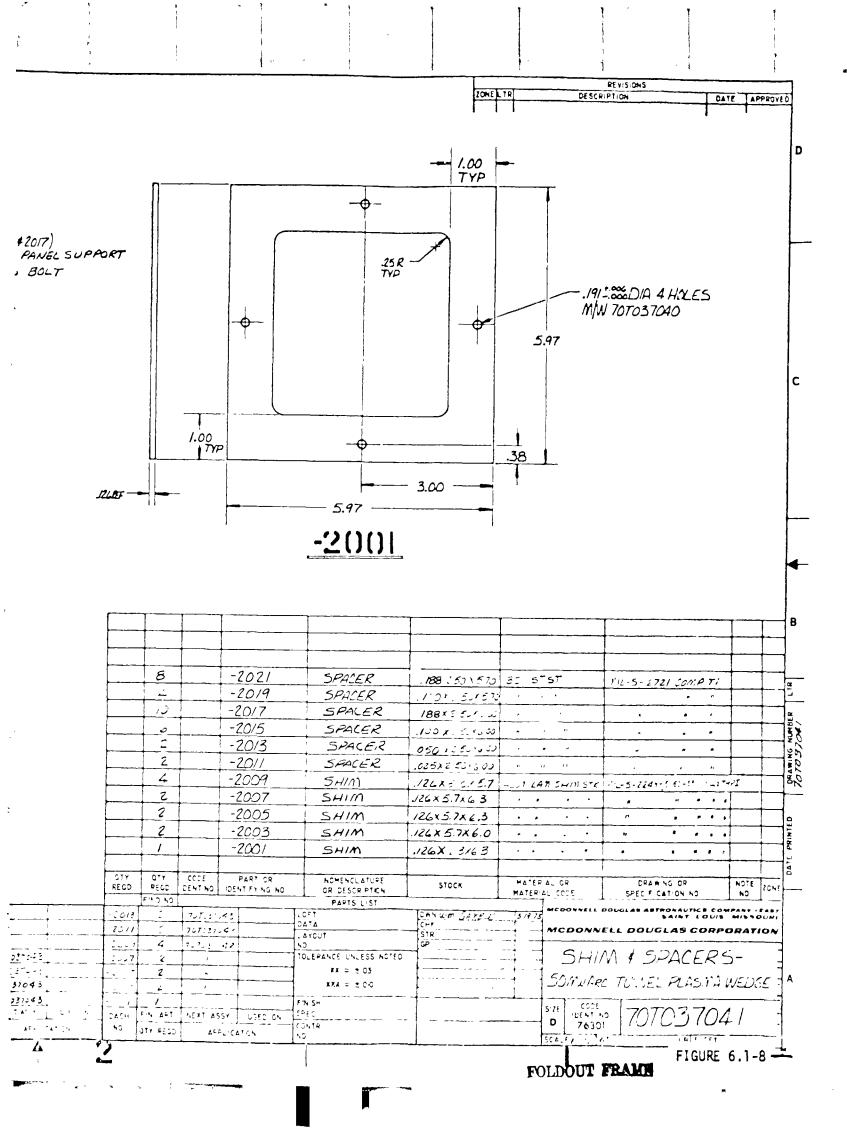


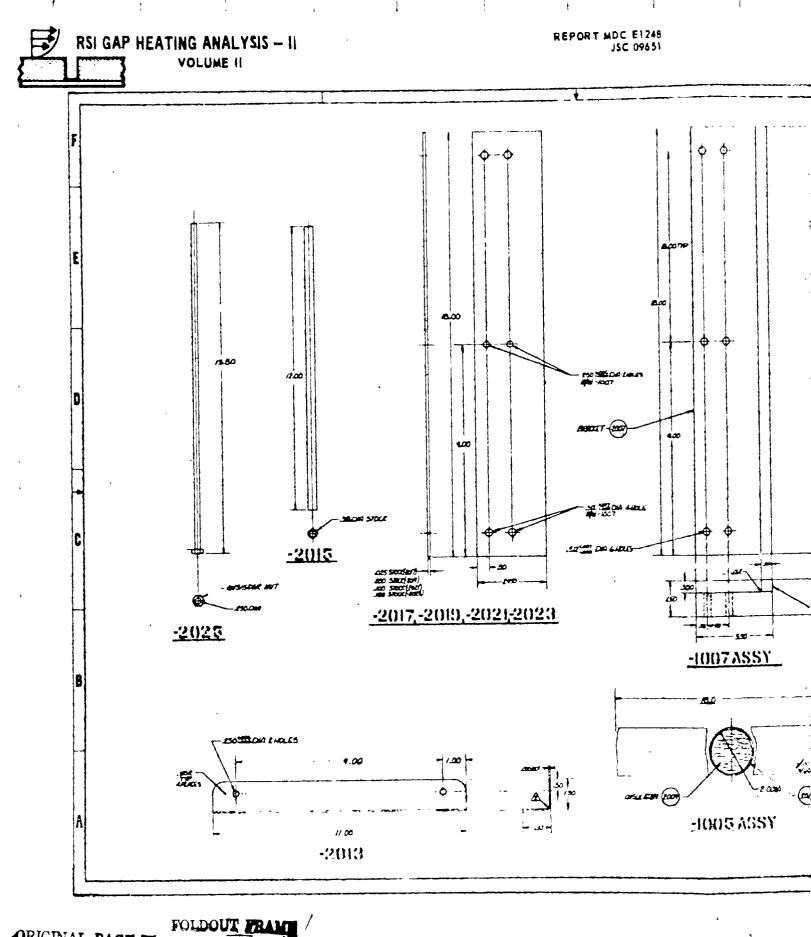


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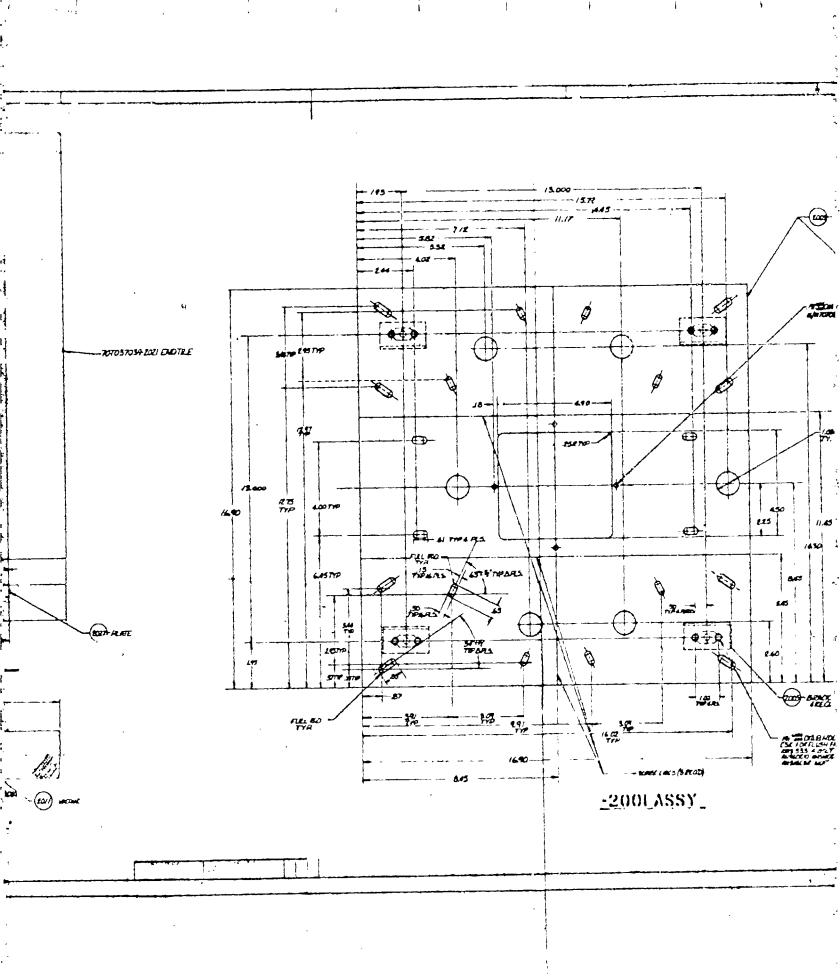




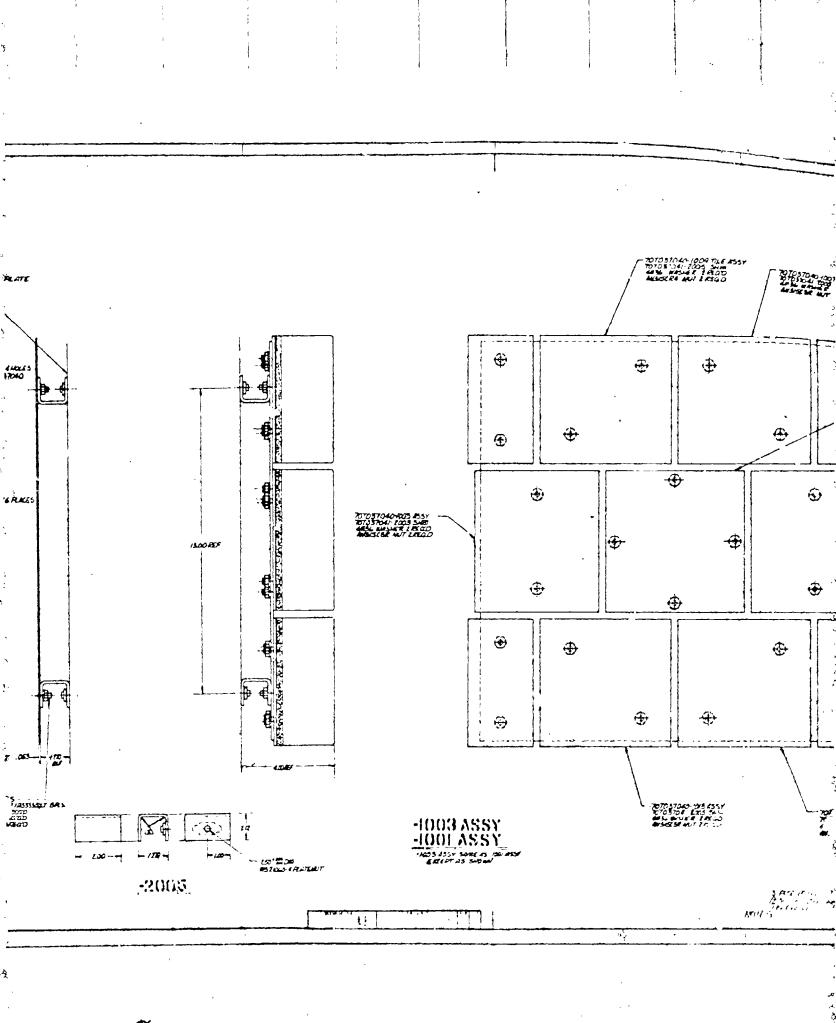


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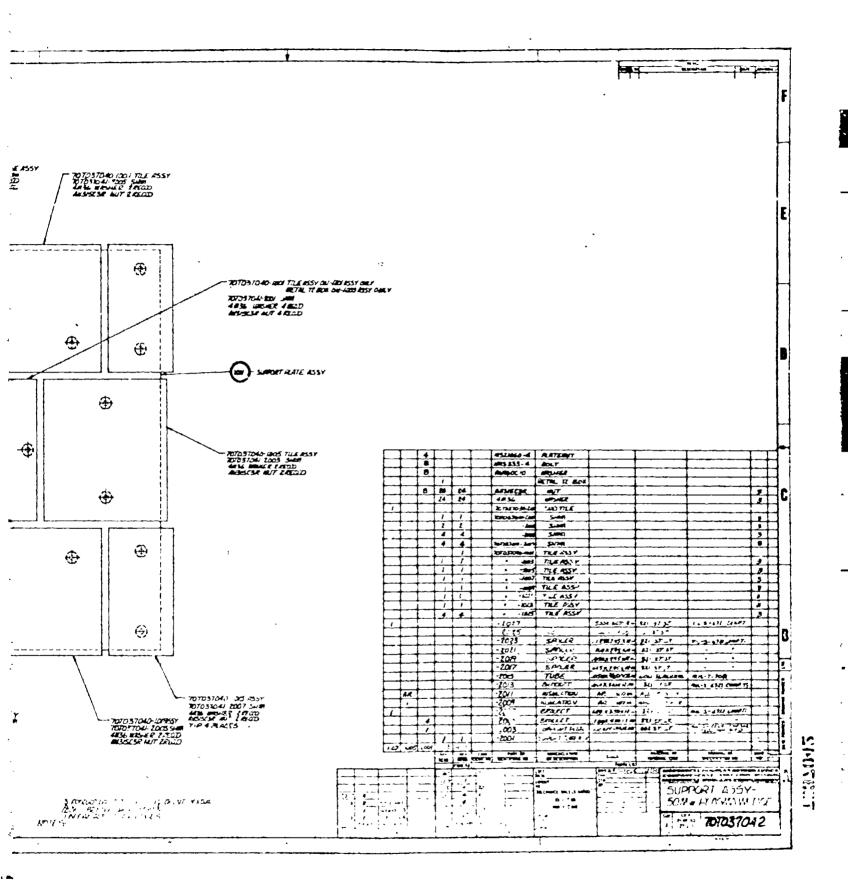
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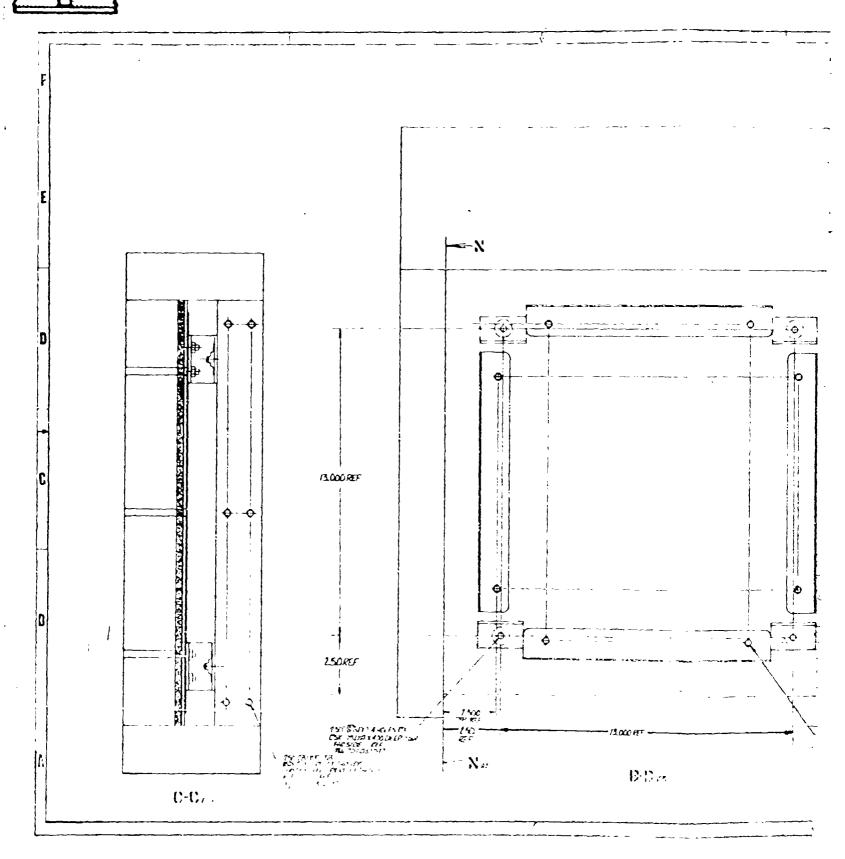


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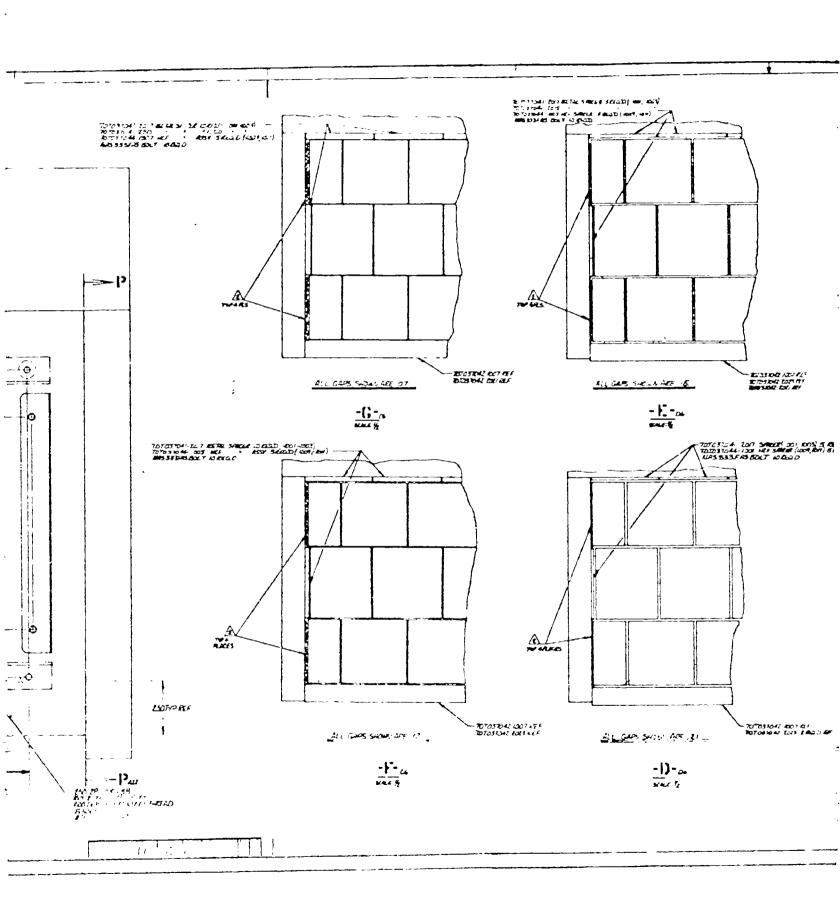
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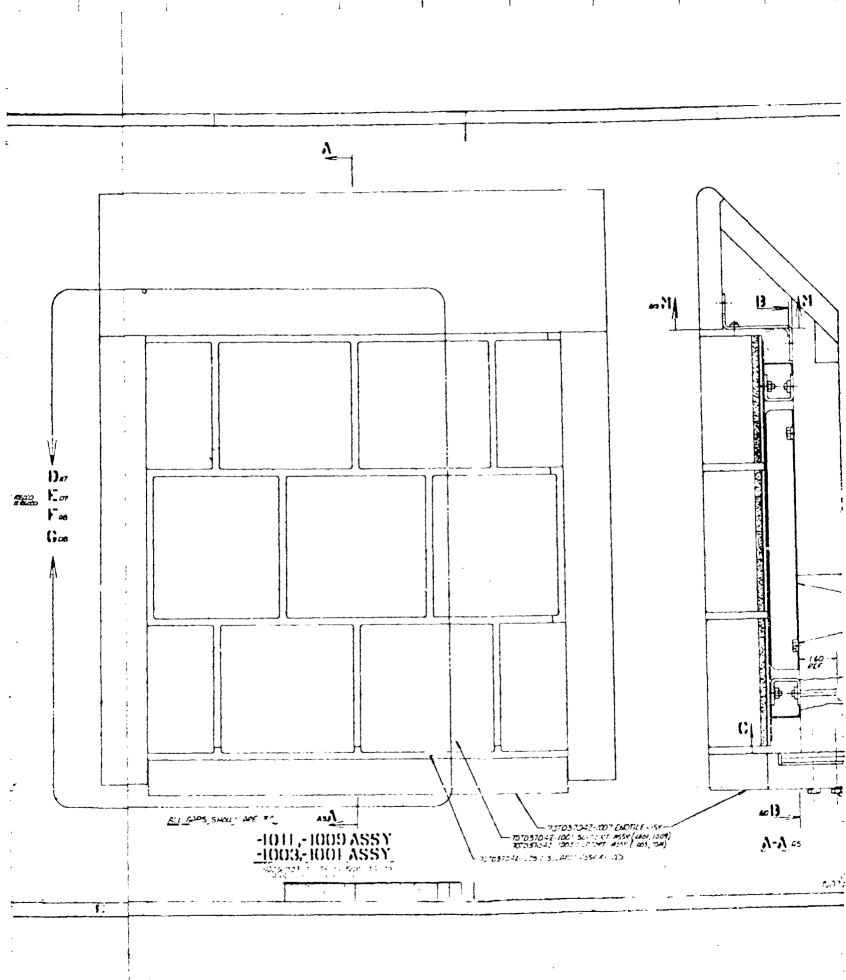
FIGURE 6.1-9



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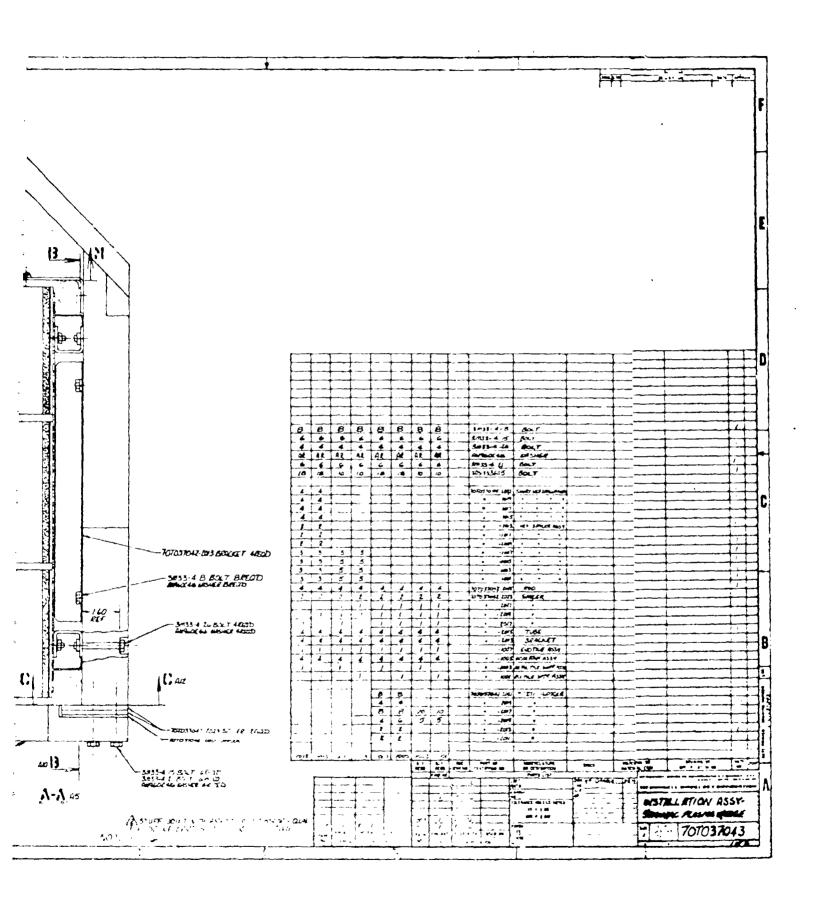
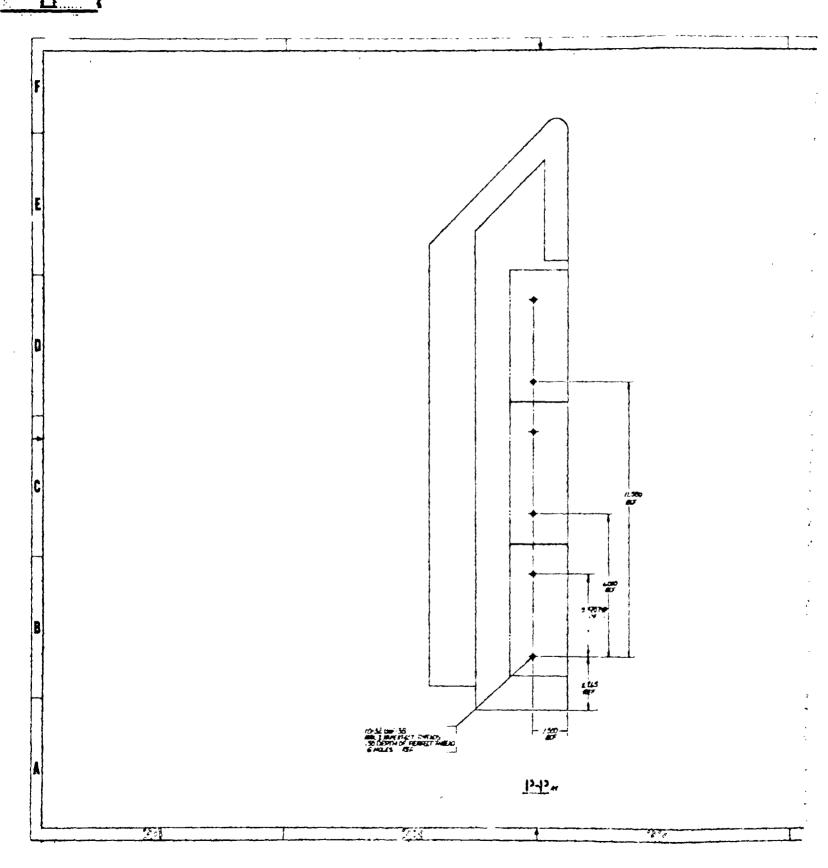
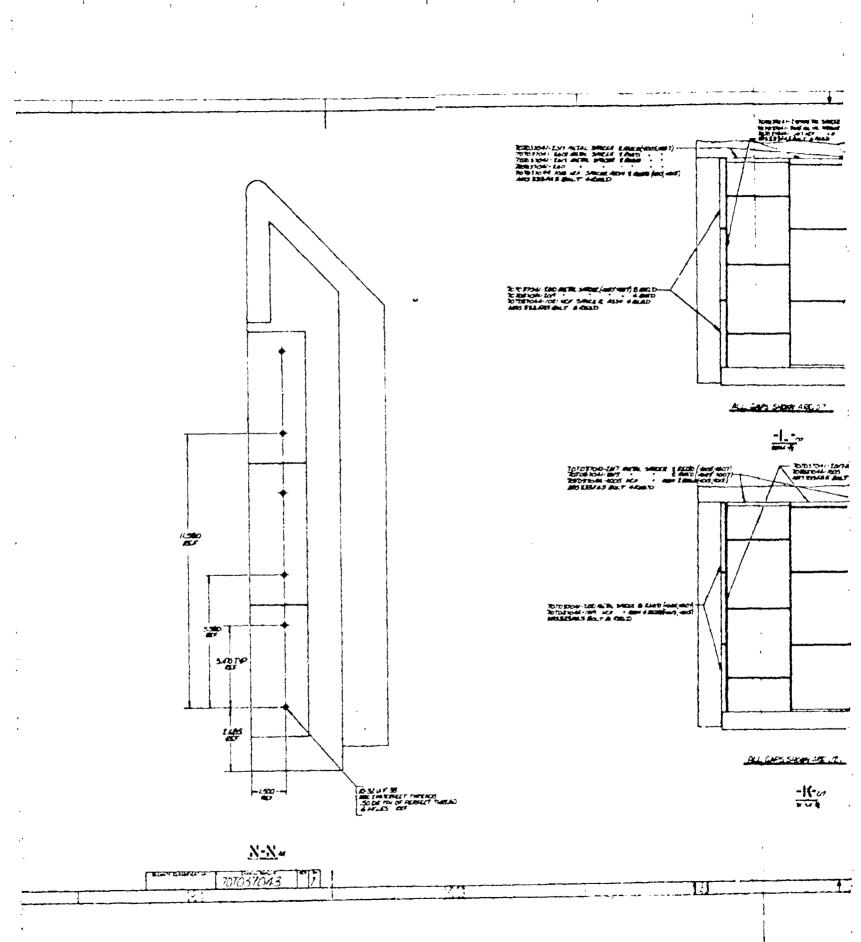
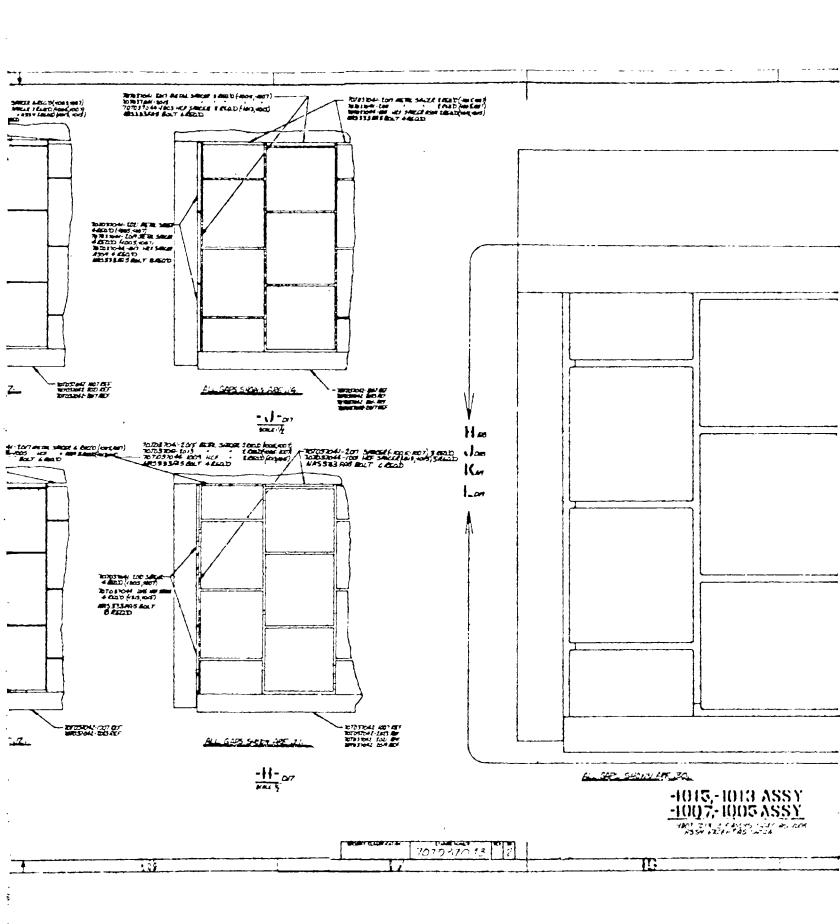


FIGURE 6.1-10





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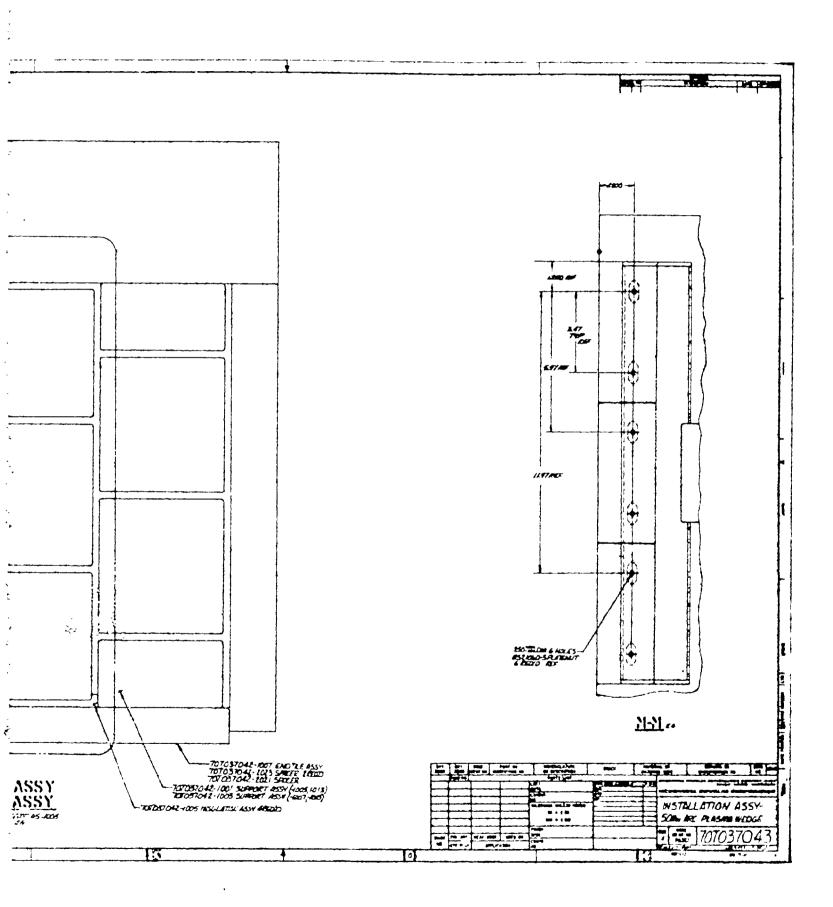
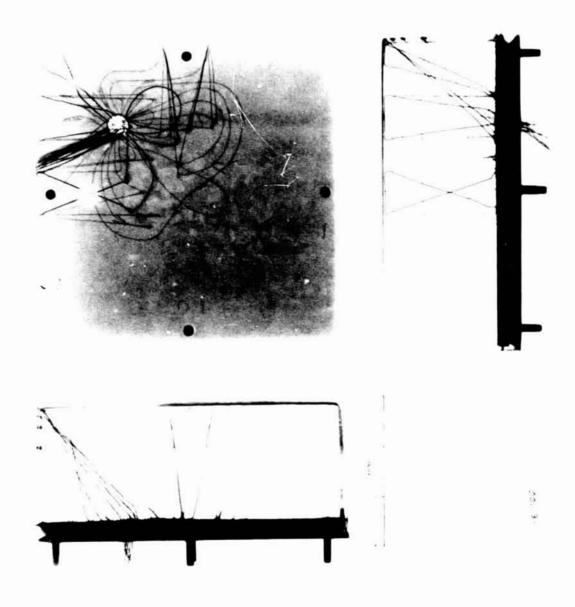


FIGURE 6.1-10 CONC.



#### RADIOGRAPH OF TILE ASSEMBLY 1001-31 46x46 CM RSI GAP HEATING EVALUATION PANEL



REPORT MDC E1248 JSC 09651

#### RADIOGRAPH OF TILE ASSEMBLY 1003-29 46x46 CM RSI GAP HEATING EVALUATION PANEL



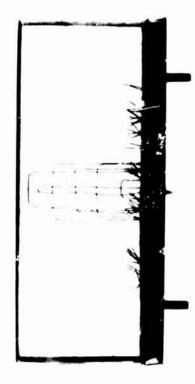
#### RADIOGRAPH OF TILE ASSEMBLY 1003-35 46x46 CM RSI GAP HEATING EVALUATION PANEL

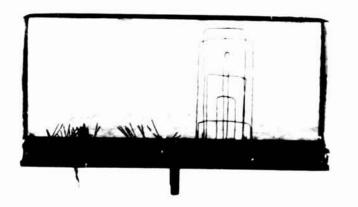
REPORT MDC E1248 JSC 09651

#### RADIOGRAPH OF TILE ASSEMBLY 1005-20 46x46 CM RSI GAP HEATING EVALUATION PANEL

1005-20



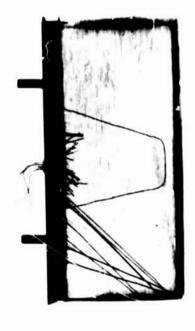


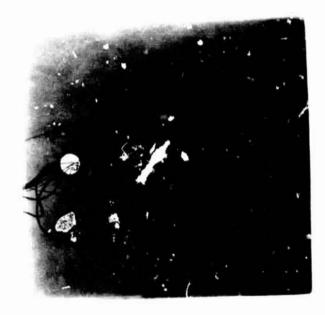


RSI GAP HEATING ANALYSIS - II

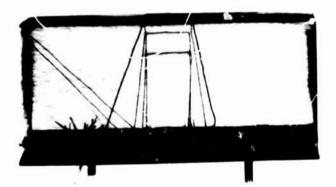
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#### RADIOGRAPH OF TILE ASSEMBLY 1007-30 46x46CM RSI GAP HEATING EVALUATION PANEL



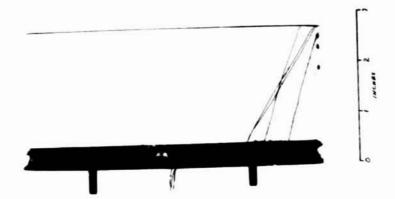






## RADIOGRAPH OF TILE ASSEMBLY 1009-28 46x46 CM RSI GAP HEATING EVALUATION PANEL

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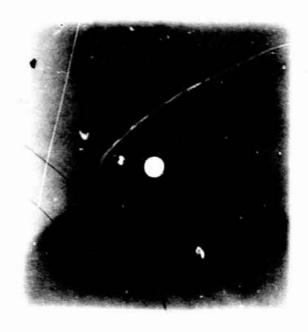
RSI GAP HEATING ANALYSIS - II

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## RADIOGRAPH OF TILE ASSEMBLY 1011-26 46x46 CM RSI GAP HEATING EVALUATION PANEL

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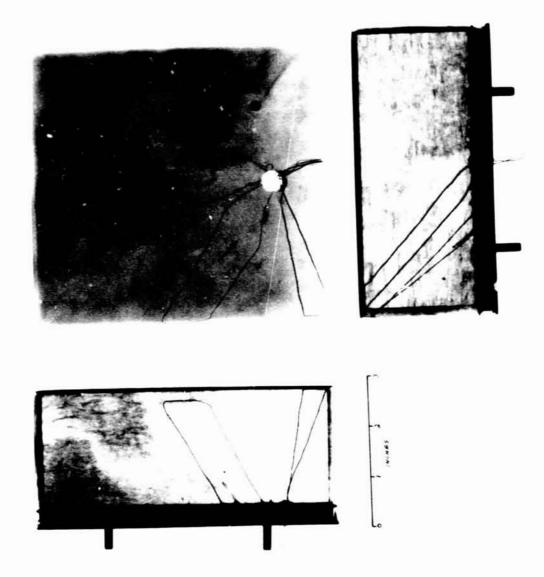






## RADIOGRAPH OF TILE ASSEMBLY 1013-19 46x46 CM RSI GAP HEATING EVALUATION PANEL

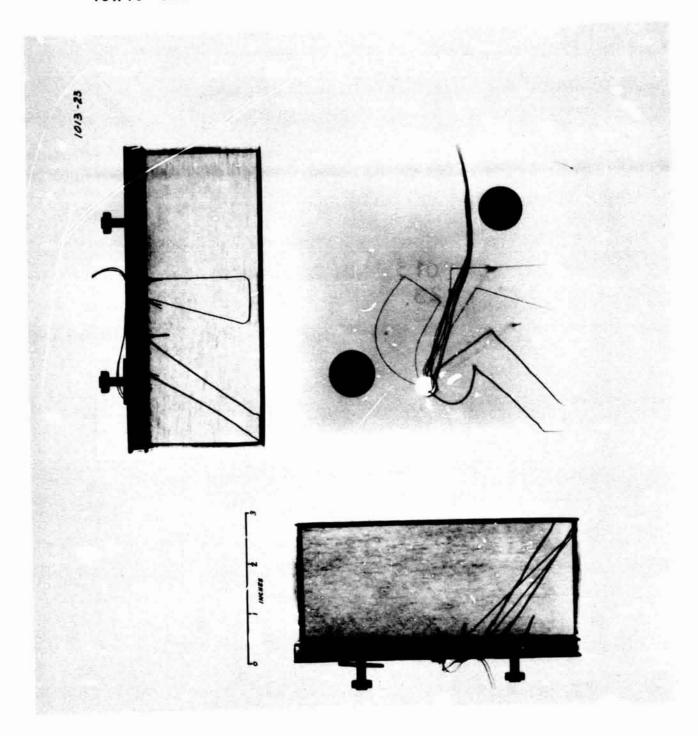
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RSI GAP HEATING ANALYSIS - II

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## RADIOGRAPH OF TILE ASSEMBLY 1013-23 46x46 CM RSI GAP HEATING EVALUATION PANEL





6.2 Explanation of Terminology Used in Data Listing - Results from the HTST tests presented in Section 6.3 are organized by run number and contain information about test conditions, model configuration and thermocouple location, heat transfer parameters and boundary layer parameters. The data listing was prepared by analyzing and combining information recorded during calibration and test runs with boundary layer information.

The terminology used in the data listing is as follows:

TT = Free stream total temperature

PTC = Combustor pressure

TAW - Adiabatic wall temperature

MACH = Mach number

PT(I) - Total pressure ahead of normal shock

P(F) - Free stream pressure

T(FS) = Free stream temperature

D-PRESS(FS) = Free stream dynamic pressure

(RHO-V)FS - Product of free stream density and velocity

(CP-RHO-V)FS - Product of free stream specific heat, density, and velocity

(RHO-TAU-CP)M = Product of metal tile density, thickness, and specific heat

RE/METER = Free stream Reynolds number

H(FLAT PLATE) = Tunnel reference flat plate heat transfer coefficient

TTIME = Test time at which computations were obtained

STEP = Step height
GAP = Gap width

CP(GAS) = Gas specific heat

RECOVERY FACTOR - TAW/TT

T/C = Thermocouple number

CH = Channel number

X --- X-coordinate of instrumentation point, origin at center of tile

Y - Y-coordinate of instrumentation point, origin at center of tile

Z = Distance from top of tile (X, Y, Z for right hand coordinate

system)

XBAR = Surface distance from tile center

YBAR - Lateral surface distance from tile center

Convective heating rate PRECEDING PAGE BLANK NOT FILLE



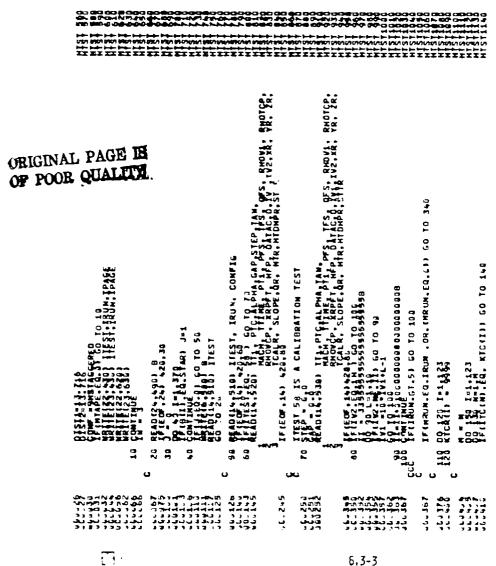
HT	Turbulent convective	heat transfer coefficient (0.912 recovery
	factor), uncorrected	
HTDHP	Heat transfer ratioed	to theoretical flat plate heat transfer
	coefficient, uncorrec	ted.
HT/HF	Convective heat trans	fer ratioed to calibration plate heating
NSTT	Stanton number based	on free stream conditions and HT
T	Local temperature rec	orded on the thin skin tile at TTIME
HTC/HF	Conduction corrected	HT ratioed to calibration plate heating
HTC/HEC	Conduction corrected	HT ratioed to heat transfer coefficient
	on tile surface near	gap (conduction corrected)
HT/H-CNTR	Heat transfer coeffic	eient ratioed to heat transfer coefficient
	at center of tile	



6.3 Data Tabulation for LaRC 8 Foot HTST Gap Heating Tests - This section contains the program for transcribing data from the HTST into the Data Bank and the tabulation generated by the program. The program listing is included for completeness and also documents those steps necessary to process the data into the Data Bank. The data listing begins on Page 6.3-26. This listing employs the "24 Attribute Word List" (described in Volume I, Section 5) used in the data selection and data correlation programs.

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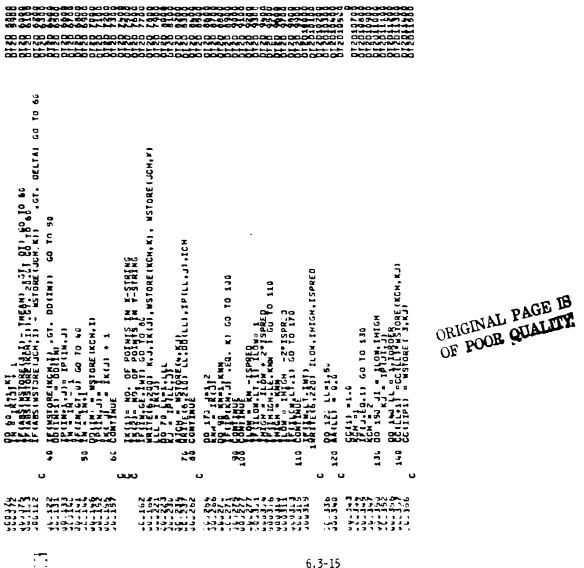
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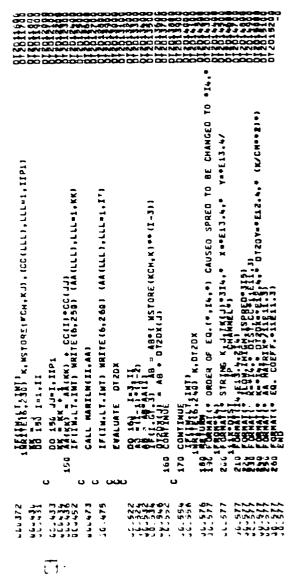
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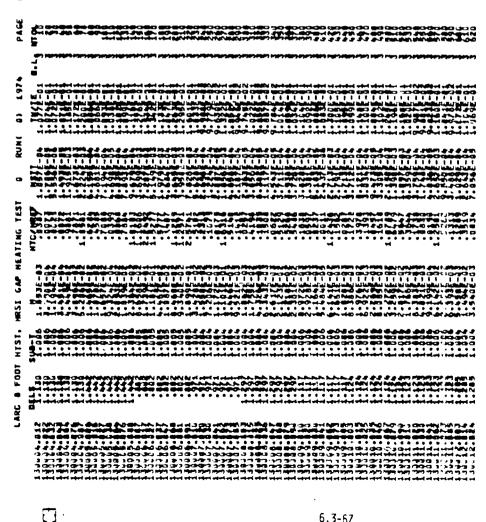
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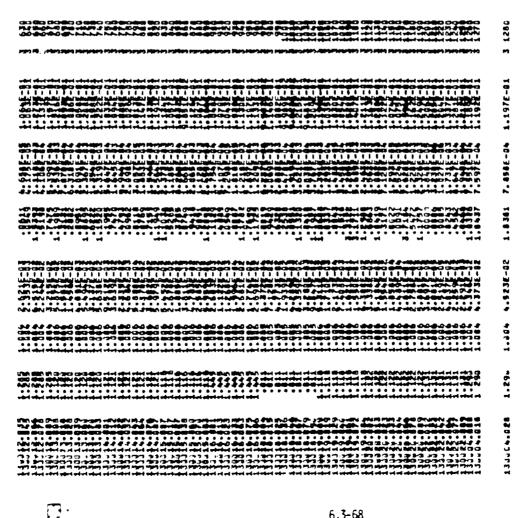
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#### 7.0 NASA-JSC 10 MW ARC TUNNEL EDGE RADIUS TESTS

Gap heating tests were conducted by C. D. Scott (NASA, Johnson Space Center) in the JSC 10 MW Arc Tunnel to provide heating data in the presence of a high enthalpy laminar boundary layer. The test parameters, model description and data were obtained from Reference 4. The 50.8 cm diameter conical nozzle produced the flow field. The test parameters are shown below and conditions on the wedge are shown on Figure 7.0-1. The primary purpose of the tests was to investigate the effect of tile edge radius on gap heating.

The tests employed sets of thin skin metallic tiles mounted in a wedge test fixture shown on Figure 7.0-2. Four edge radii (0.157, 0.3175, 0.635, and 1.27 cm) were parametrically tested at gap widths of 0.127, 0.254, and 0.381 cm, at 15° angle of attack. The joint configuration was an in-line butt, and the tile height was 4.1275 cm for all tests. During each run the model was inserted three times into the flow for approximately three seconds each while the thermocouple responded to the incident heating. The reported data are averages of the three measurements. The reference model and pitot pressure probe were inserted into the flow during each run to determine the repeatability of the test condition. A run schedule is shown on Figure 7.0-3. The reference model, flat surface without gaps, instrumented with Gardon gauge calorimeters was used to measure reference heating rates.

#### TEST PARAMETERS

MACH NO.	9.6
ANGLE OF ATTACK, DEG.	15.0
TOTAL ENTHALPY, M1/K8	13.9
REYNOLDS NO./METER	1741.0
PITOT PRESSURE, N/M <sup>2</sup>	145.0

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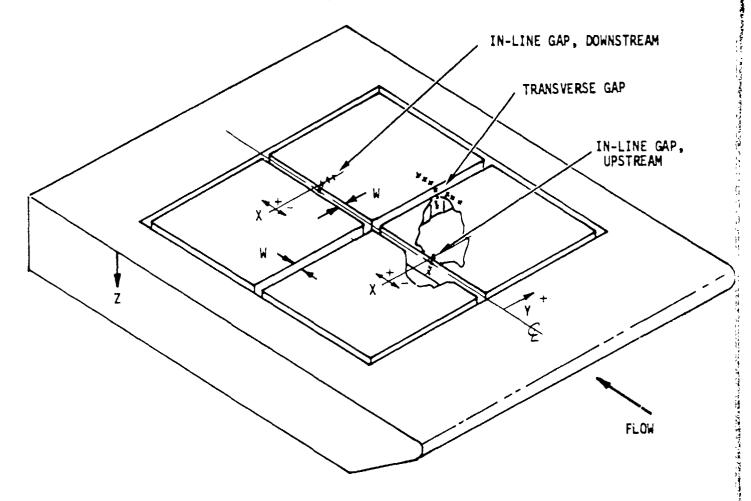
CONDITIONS

Displacement Thickness	CB	11.	.95		1.22		1.44	1.54
Measured Heat Flux	W/cm <sup>2</sup>			10.44	8.62	7.49		
Calculated Heat Flux	W/cm <sup>2</sup>	11.12	90.6		7.02		5.95	5.57
Calculated Pressure	N/m <sup>2</sup>	265.	242.		220.		208.	204.
Distance from Leading Edge* of Tiles	Cm	0	5.04	7.62	15.24	22.86	25.40	30.48
Distance from Leading Edge* of Wedge	сш	10.92	16.15		26.4		36.6	41.7

\*Leading Edge Radius = 0.95 cm

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## TEST PANEL CONFIGURATION, EDGE RADIUS STUDY AT NASA JSC 10 MW ARC TUNNEL





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### JSC 10 MW RUN SCHEDULE FOR EDGE RADIUS TESTS

RUN	EDGE RADIUS (cm)	GAP WIDTH (cm)
779	0.1575	0.127
780		0.381
781	•	0.254
782	0.3175	0.127
783		0.254
784	<b>\</b>	0.381
785	0.635	0.127
786		0.254
787	₩	0.381
788	1.27	0.127
789		0.254
790		0.381



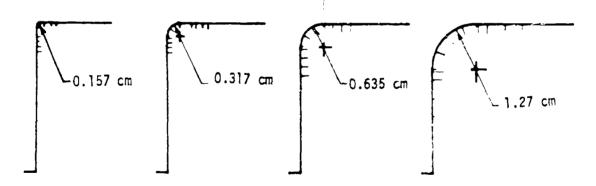
7.1 Model Description - The test article consists of 15.24 cm square stain-less steel tiles with various edge radii mounted in a wedge (15° angle-of-attack), Figure 7.0-2. The parametric variation of edga radii was 0.1575, 0.3175, 0.635, and 1.27 centimeters with gap widths of 0.127, 0.254, and 0.381 centimeters. The tiles were aligned in an "in-line" arrangement, thereby creating gaps both perpendicular and parallel to the flow direction. Thermocouples were attached to the inner surface of the tiles in a row around the gap shown in Figure 7.0-2. Figure 7.1-1 shows the nominal locations of Sets of instrumentation on the gaps and also shows the locations of thermocouples on a Set for various edge radii.

The thickness of the skin is about .029 inch on the upper surface and rounded edge of the tiles, while it is about .010 inch on the sides of the tiles. Forty-gauge iron-constantan thermocouples were attached to the thin areas and 36-gauge chromel-alumel were attached to the thicker areas. The ratio of wire diameter to skin thickness was chosen to minimize the effects of conduction along the wires. The inside of the tiles were packed with fibrous silica to minimize cross radiative effects.

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# NOMINAL LOCATIONS OF SETS OF INSTRUMENTATION ON THE GAPS

Description	X CM	Y CM
Longitudinal Gap (upstream)	7.62	0
Longitudinal Gap (Downstream)	22.86	C
Transverse Gap Upstream Side	15.34	7.62
Transverse Gap Downstream Side	15.34	7.62



NOMINAL T/C LOCATIONS INDICATED BY TICK MARKS



7.2 Explanation of Terminology Used in Data Listing - Results from the 10 MW Arc Tunnel edge radius tests presented in Section 7.3 are organized by instrumentation location and within each location are segregated by edge radius and gap width. The data listing was prepared by analyzing and combining information recorded during calibration and test runs.

The terminology used in the data listing is as follows:

TEST-RUN-T/C = Test, run and thermocouple numbers

G-CF = Gap configuration

LOC = Instrumentation location

X = X coordinate of instrumentation point, origin at center

of tile (see Figure 7.0-2)

Y = Y coordinate of instrumentation point, origin at centerline

between tiles (see Figure 7.0-2)

Z = Distance from top of tile (see Figure 7.0-2)

X(BAR) = Distance from leading edge of tile

E = Tile edge radius

GAMMA = Flow orientation

GAP = Gap width

STEP = Step height

FLOW = Gap flow length

PATN = Tile pattern (0=staggered, 1=in-line)

M = Mach number

RE/METER = Unit Reynolds number

DELS = Displacement thickness

Q/QREF = Convective heating in gap ratioed to convective heating

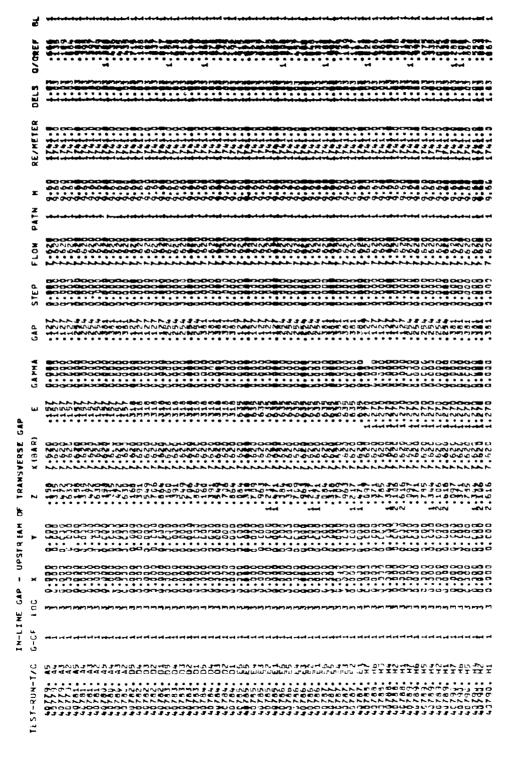
on flat plate at the same location

BL = Boundary layer state (1=laminar)

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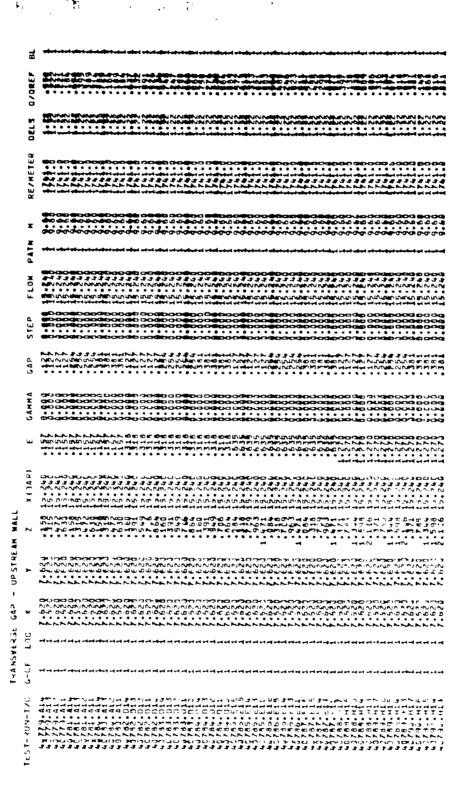
7.3 Data Tabulation for 10 MW Arc Tunnel Edge Radius Gap Heating Tests - This section contains the data from the 10 MW Arc Tunnel which is stored in the Data Bank. The data listing begins on Page 7.3-2.

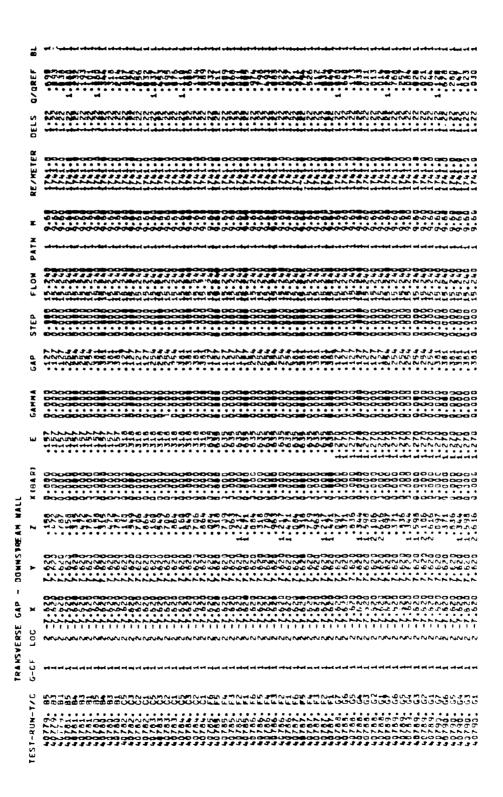
This listing employs the "24 Attribute Word List" (described in Volume 1, Section 5) used in the data selection and data correlation programs.



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